

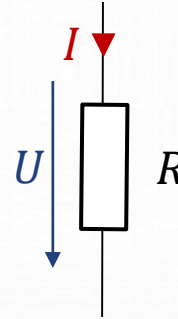
PVK ELEKTROTECHNIK 1

ABLAUF

- BASICS
- NETZWERKANALYSE
- REALE QUELLEN
- LEISTUNGSANPASSUNG
- SUPERPOSITION
- NORTON/ THÉVENIN-ÄQUIVALENT
- KONDENSATOR
- MAGNETFELD
- SPULEN
- TRANSFORMATOR
- KOMPLEXE ZAHLEN
- ZEIGER UND WECHSELSTROMRECHNUNG
- SCHWINGKREISE
- KOMPLEXE LEISTUNG

Ohmsches Gesetz [$V = \Omega \cdot A$]

$$U = R \cdot I$$

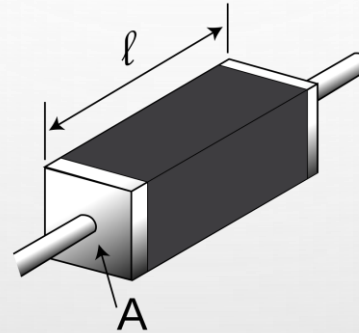


Leistung [W]

$$P = U \cdot I$$

Widerstand [Ω]

$$R = \frac{\rho l}{A}$$



Leitwert [S]

$$G = \frac{1}{R}$$

Spez. Widerstand [Ωm]

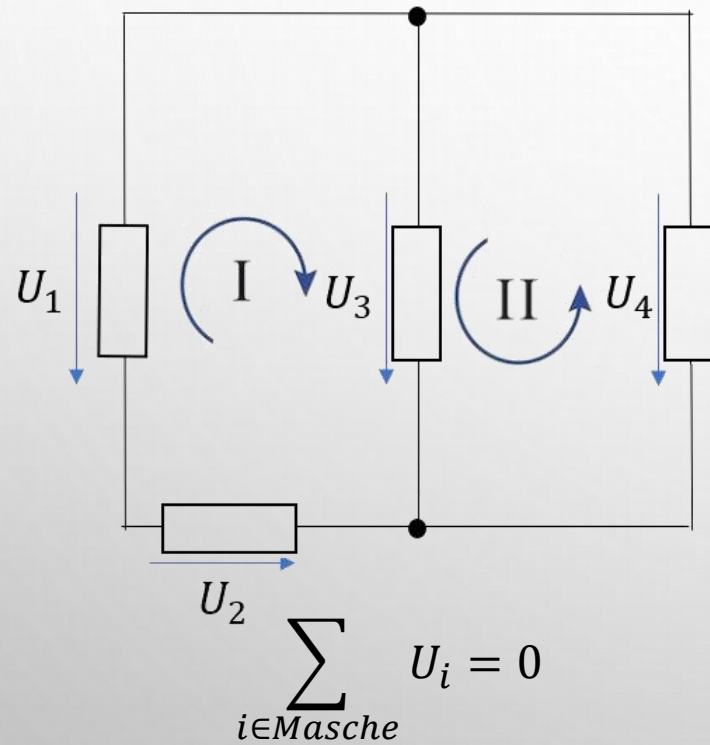
$$\rho(T) = \rho(T_0)[1 + \alpha \cdot (T - T_0)]$$

Leitfähigkeit [$\frac{S}{m}$]

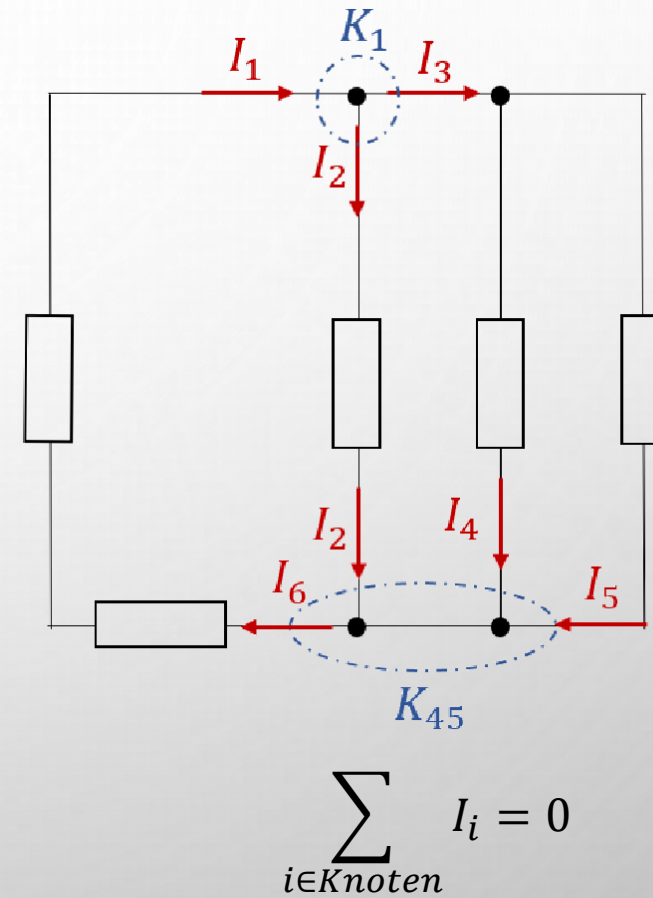
$$\kappa = \frac{1}{\rho}$$

KIRCHHOFFSCHE GESETZE

Maschenregel

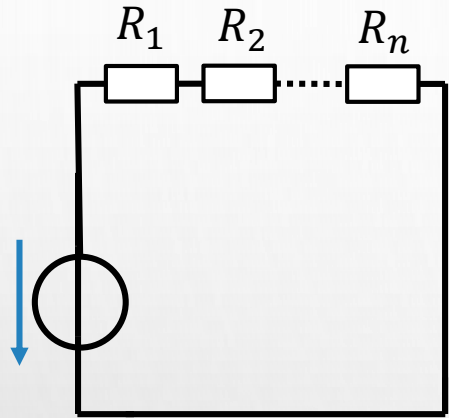


Knotenregel



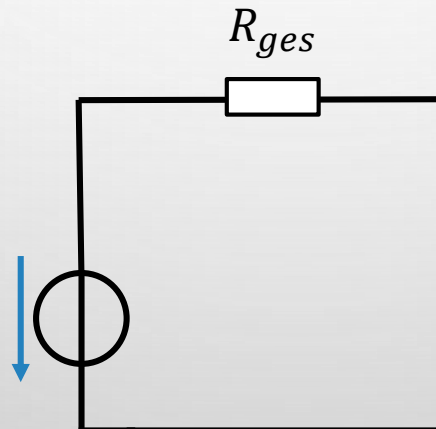
NETZWERKANALYSE

WIDERSTÄNDE



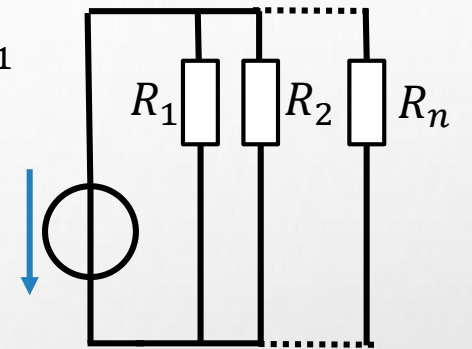
$$R_{ges} = \sum_i R_i$$

$$R_{ges} \geq \max\{R_1, \dots, R_n\}$$



$$R_{ges} = (R_1 || \dots || R_n) = \left[\sum_i Y_i \right]^{-1}$$

Nur für 2 Widerstände! $= \frac{R_1 \cdot R_2}{R_1 + R_2}$

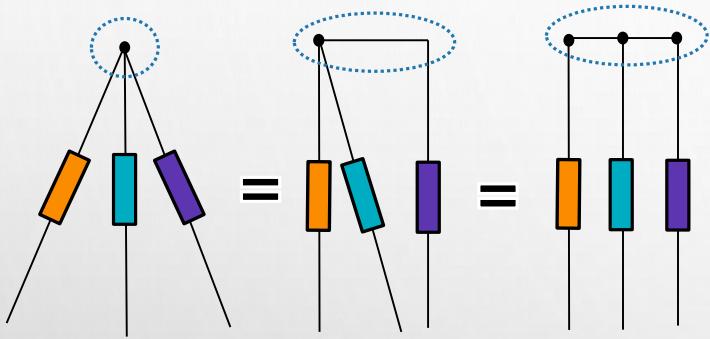


$$R_{ges} \leq \min\{R_1, \dots, R_n\}$$



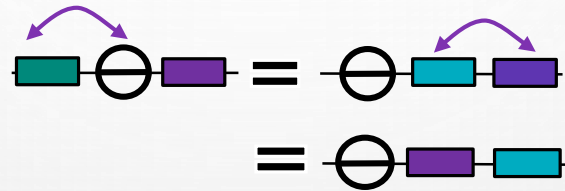
GRUNDREGELN

KNOTEN EXPANDIEREN

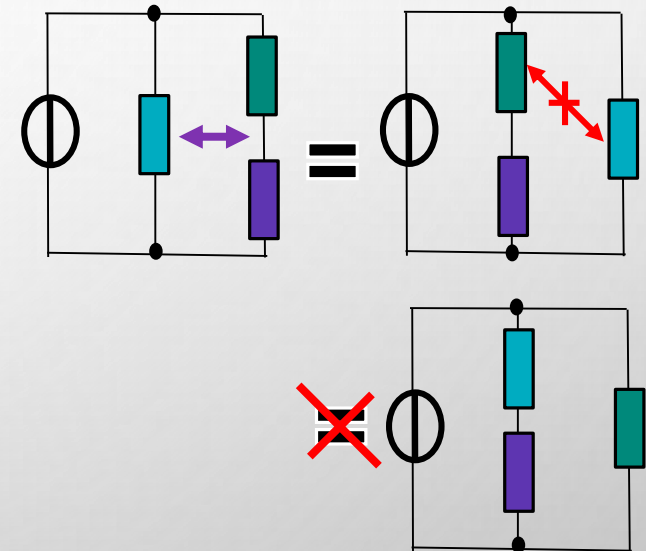


VERTAUSCHEN VON ELEMENTEN

SERIELL

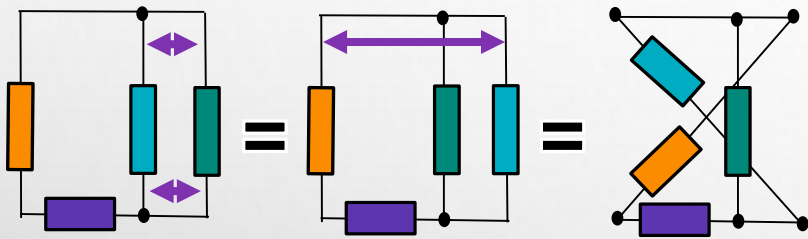


PARALLEL

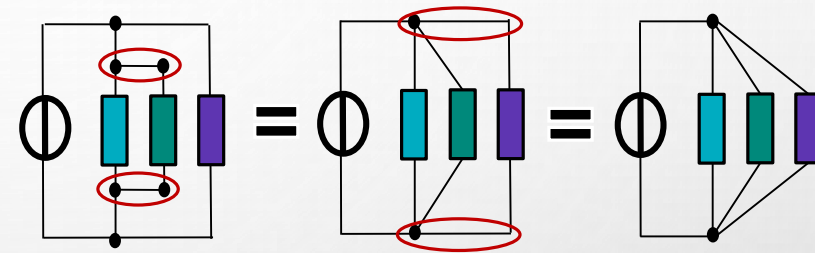


GRUNDREGELN

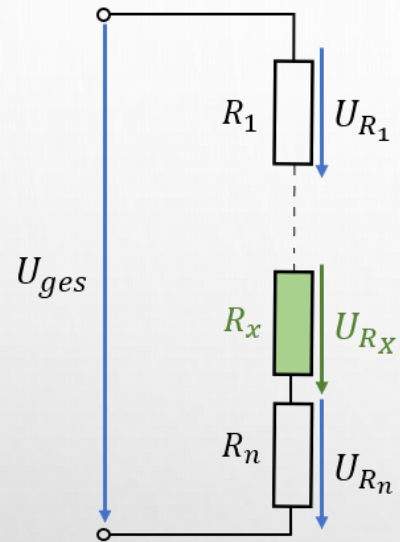
VERSCHIEBEN



KNOTEN KONTRAHIEREN

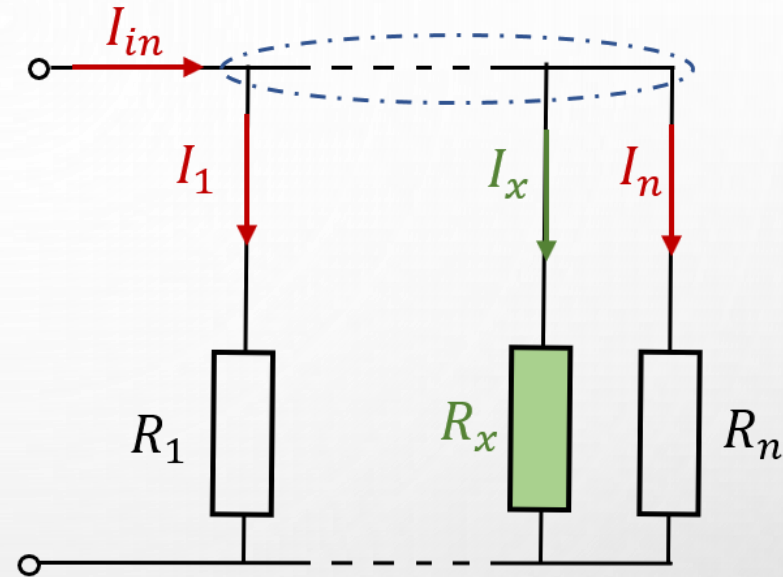


SPANNUNGSTEILER



$$U_{Rx} = U_{ges} \frac{R_x}{\sum R_i}$$

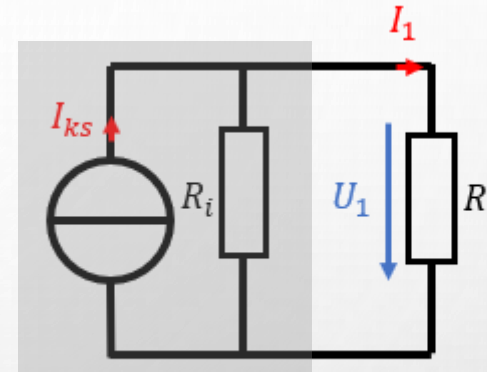
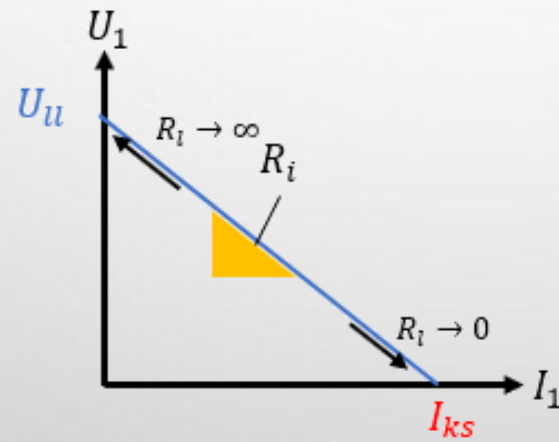
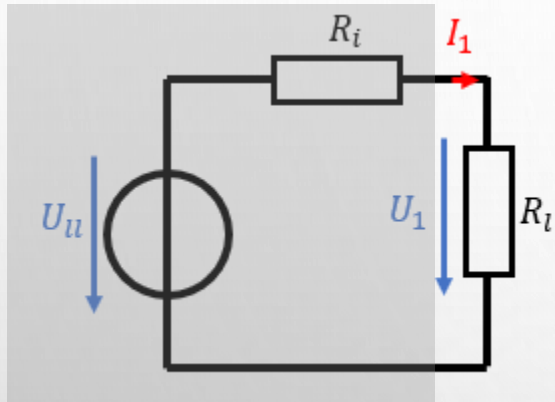
STROMTEILER

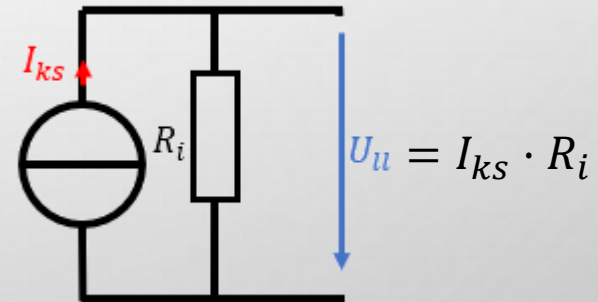
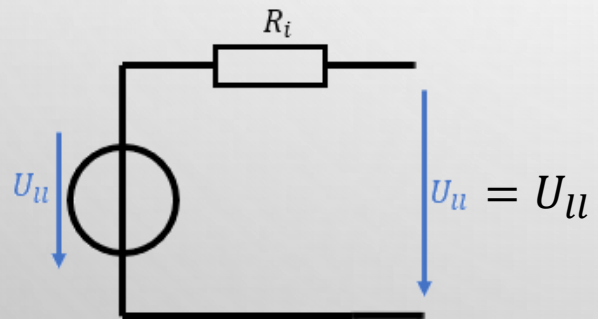
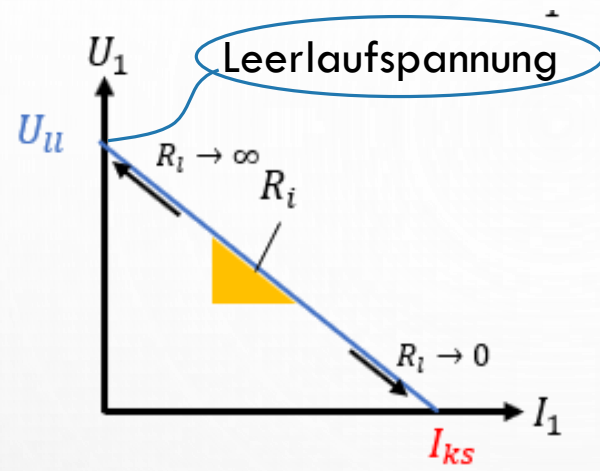


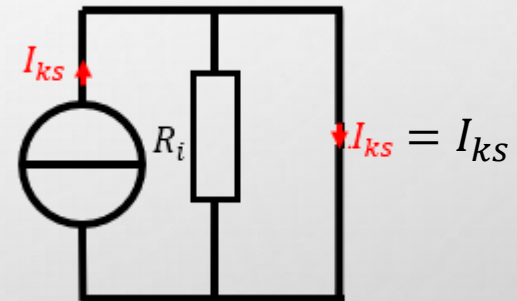
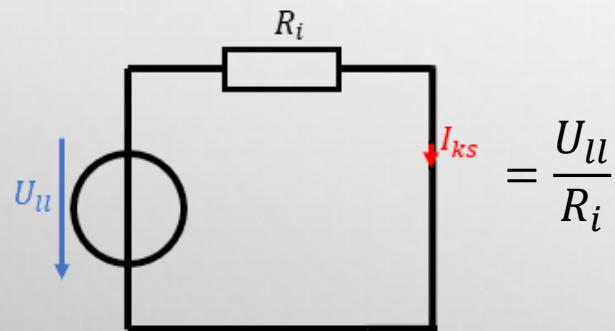
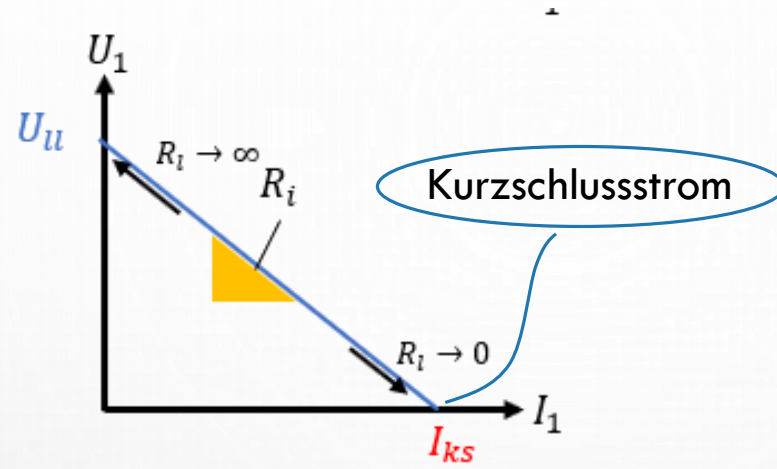
$$I_x = I_{in} \frac{(R_1 || \dots || R_n)}{R_x}$$

$$= I_{in} \frac{R_1}{R_x + R_1}$$

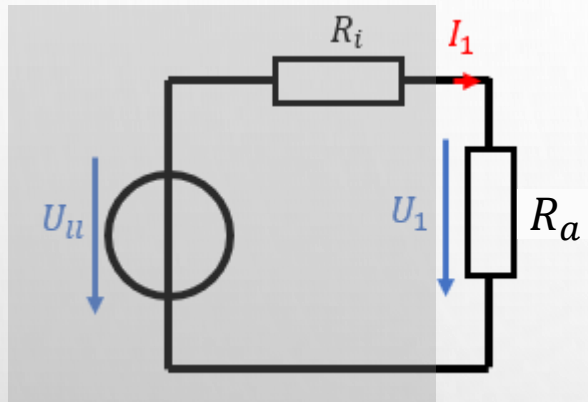
REALE QUELLEN



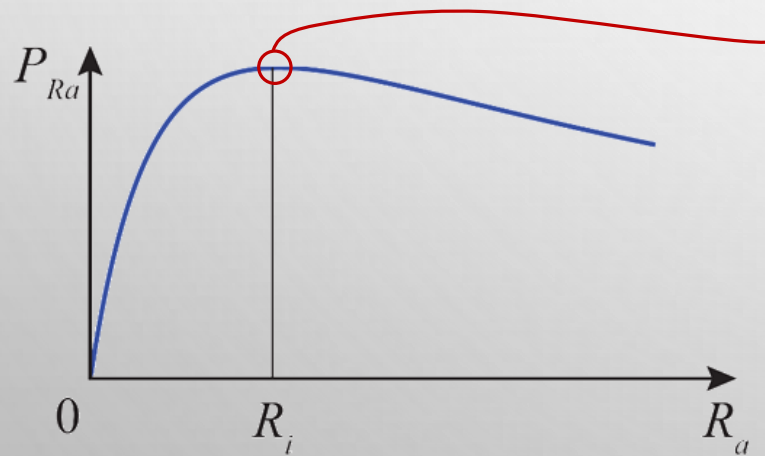




LEISTUNGSANPASSUNG



$$P_L = U_1 I_1 = \frac{U_1^2}{R_a} = \frac{\left(U_0 \frac{R_a}{R_a + R_i} \right)^2}{R_a} = U_0^2 \frac{R_a}{(R_a + R_i)^2}$$

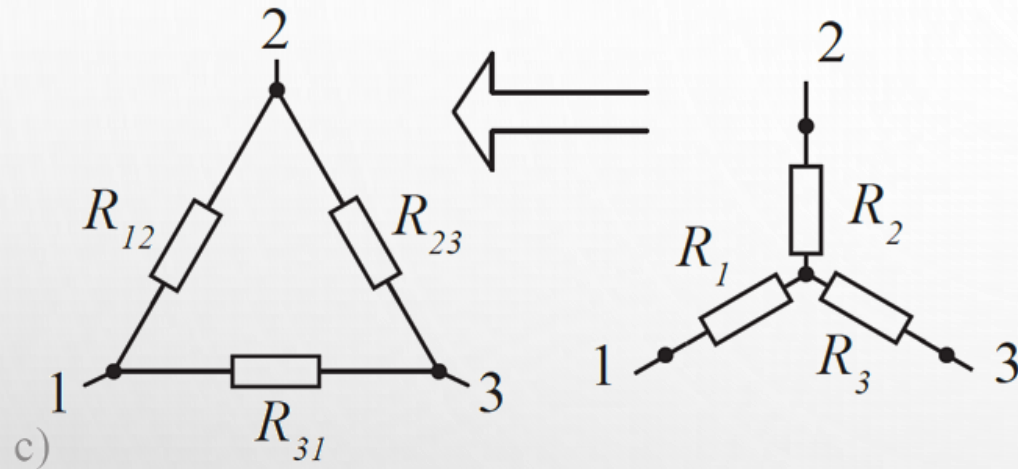


Maximale Leistung am Lastwiderstand
genau dann wenn Lastwiderstand
gleich gross wie Innenwiderstand!

$$R_L = R_i$$

$$P_{L\max} = \frac{U_0^2}{4R_i}$$

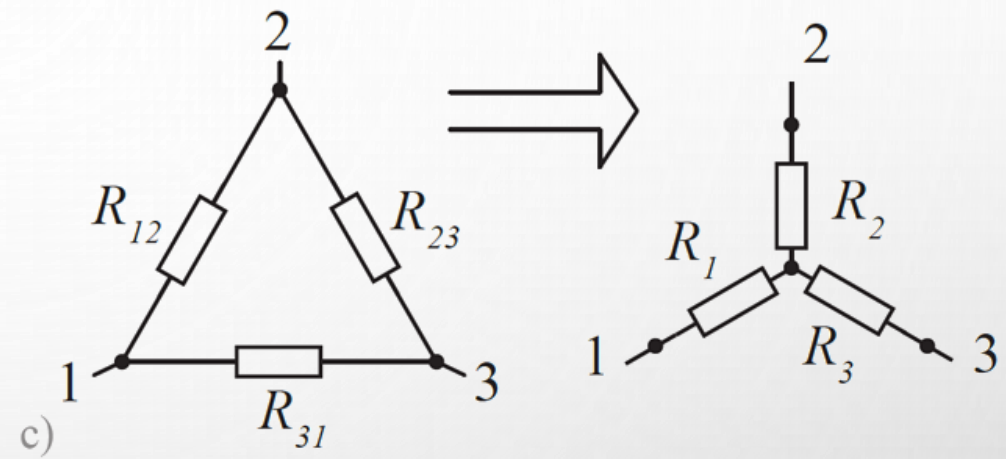
STERN-DREIECK UMFORMUNG



$$R_{12} = R_1 + R_2 + \frac{R_1 R_2}{R_3}$$

$$R_{23} = R_2 + R_3 + \frac{R_2 R_3}{R_1}$$

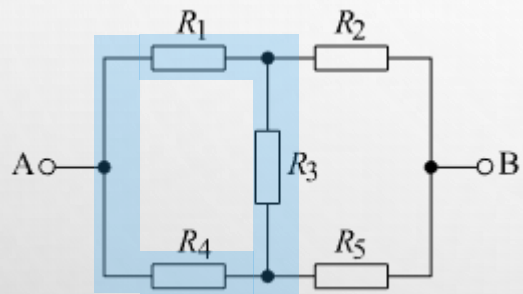
$$R_{13} = R_1 + R_3 + \frac{R_1 R_3}{R_2}$$

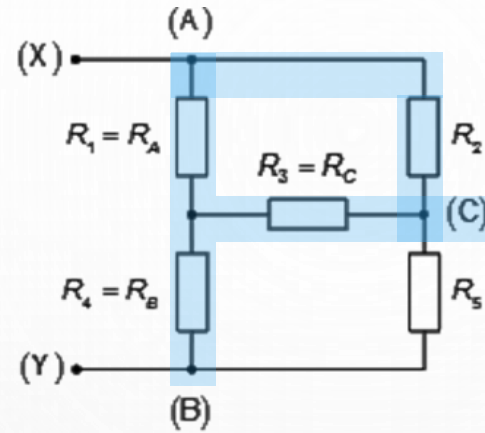


$$R_1 = \frac{R_{12} R_{31}}{R_{12} + R_{23} + R_{31}}$$

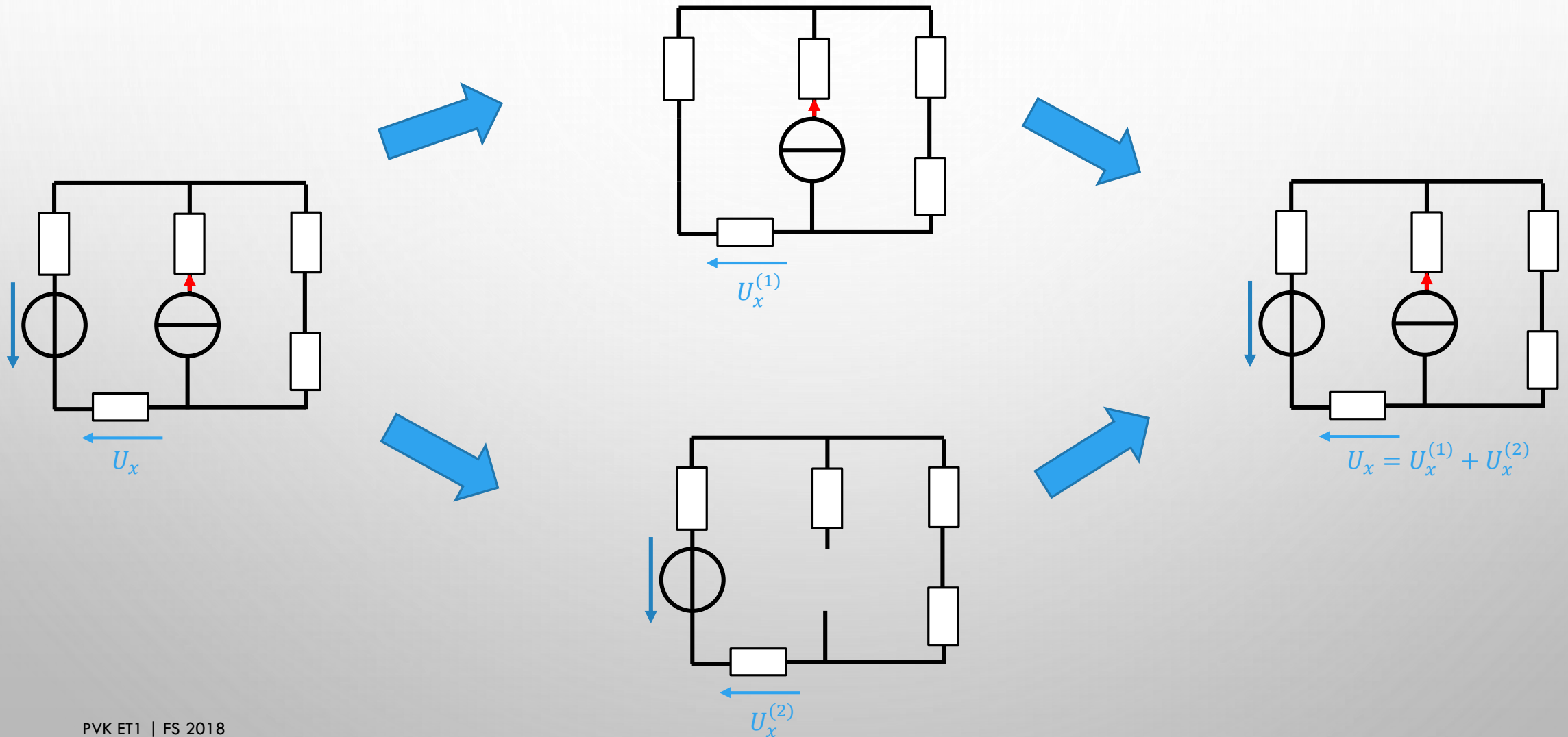
$$R_2 = \frac{R_{12} R_{23}}{R_{12} + R_{23} + R_{31}}$$

$$R_3 = \frac{R_{31} R_{23}}{R_{12} + R_{23} + R_{31}}$$

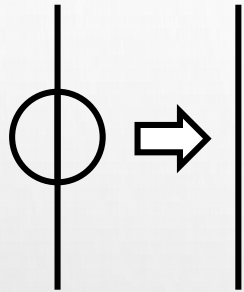




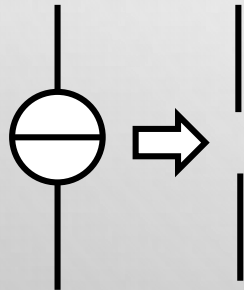
SUPERPOSITION



QUELLEN ZU NULL SETZEN

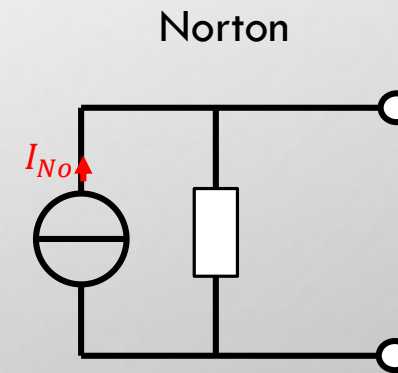
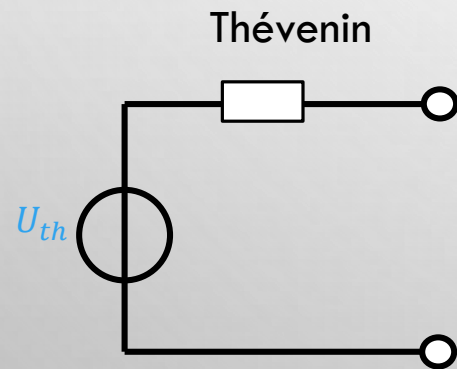
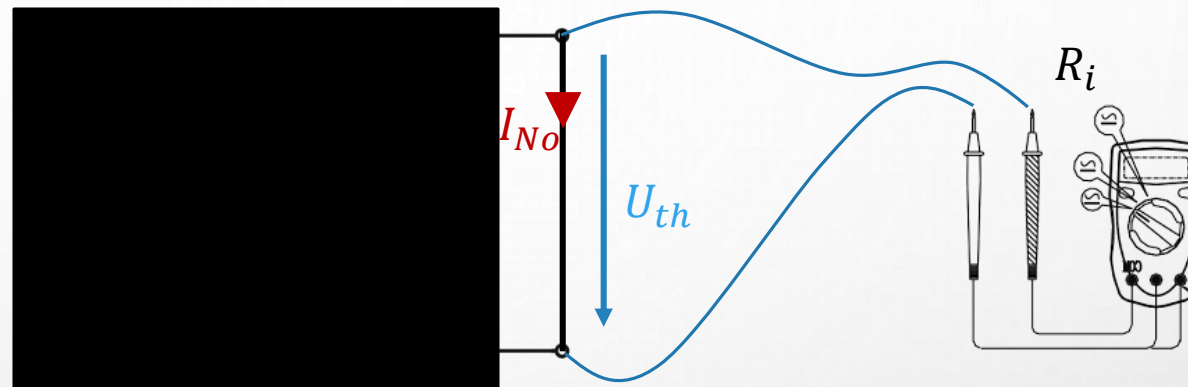


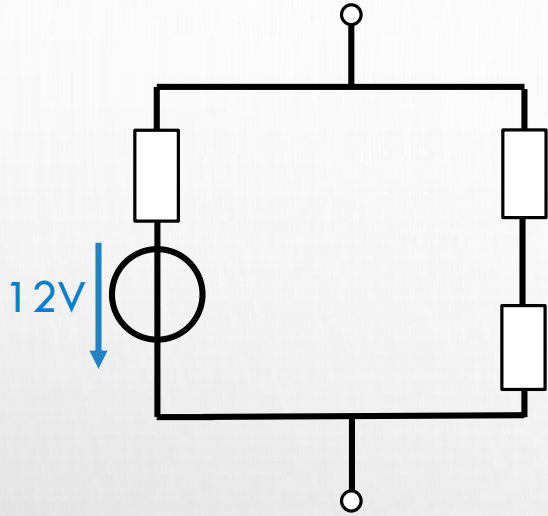
«Über einem Kurzschluss kann keine Spannung abfallen»



«Durch einen Leerlauf kann kein Strom fließen»

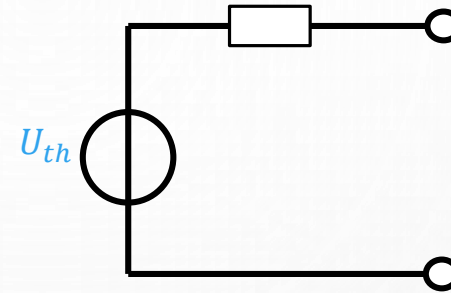
THÉVENIN / NORTON ÄQUIVALTEN





Alle Widerstände sind $1k\Omega$

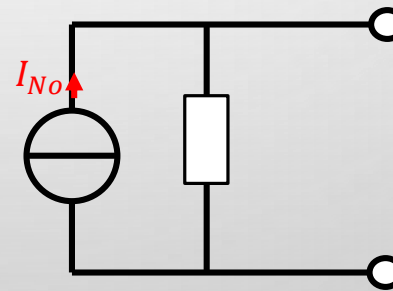
Thévenin Äquivalent



$$U_{th} =$$

$$R_i =$$

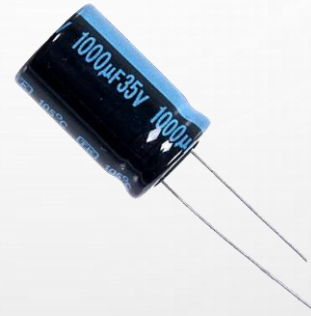
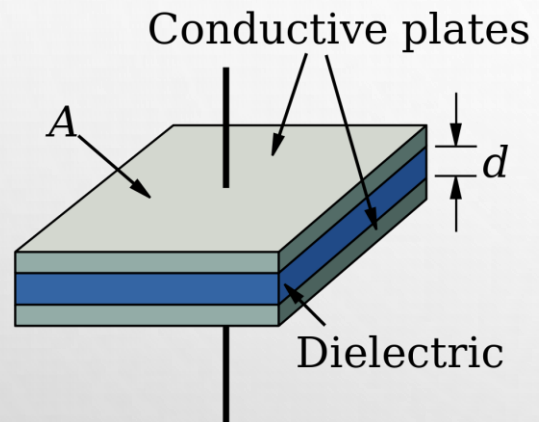
Nortin Äquivalten



$$I_{No} =$$

$$R_i =$$

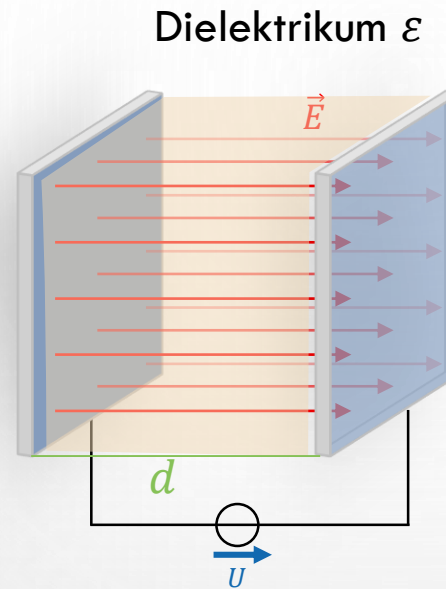
KONDENSATOR



$$\mathbf{E} = \frac{\mathbf{D}}{\varepsilon} = \frac{Q}{\varepsilon A}$$

$$U = \int \mathbf{E} \cdot d\mathbf{s}$$

$$U = d \cdot \mathbf{E} = d \cdot \frac{Q}{\varepsilon A}$$



$$\text{Kapazität } C = \frac{\text{\#Ladung}}{\text{Spannung}} = \frac{Q}{U} = \frac{\varepsilon A}{d}$$

CHARAKTERISTISCHE GLEICHUNGEN AM KONDENSATOR

$$C \cdot U = Q$$

$$C \cdot \frac{\partial}{\partial t} U(t) = \frac{\partial}{\partial t} Q(t)$$

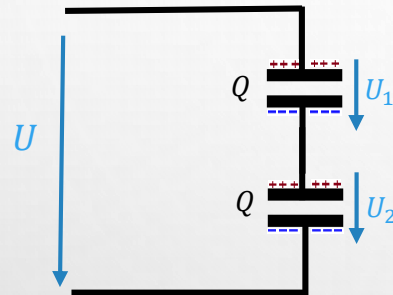
$$C \cdot \frac{\partial}{\partial t} U(t) = I(t)$$

$$C \cdot U = \int_0^t U(\tau) d\tau$$

$$W = \frac{1}{2} C \cdot U(t)^2$$

KONDENSATORSCHALTUNGEN

Serienschaltung



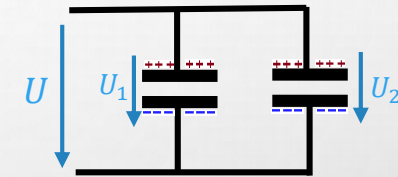
$$C_{tot} = \frac{C_1 C_2}{C_1 + C_2}$$

(für zwei Kondensatoren,
vgl. parallele Widerstände)

Gleiche Ladung
auf allen Platten!!

$$C = \frac{U}{Q} = \frac{\epsilon A}{d}$$

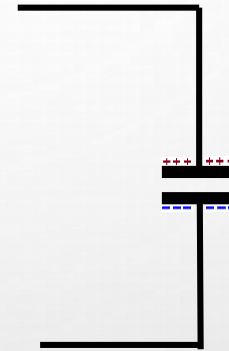
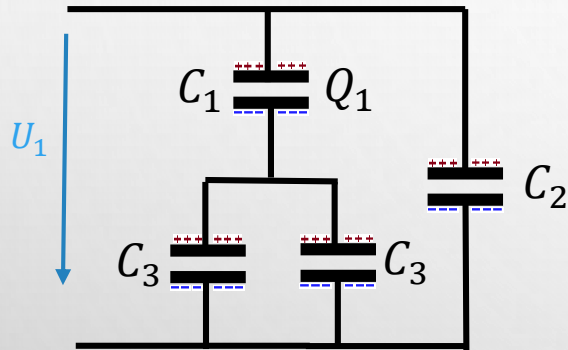
Parallelschaltung



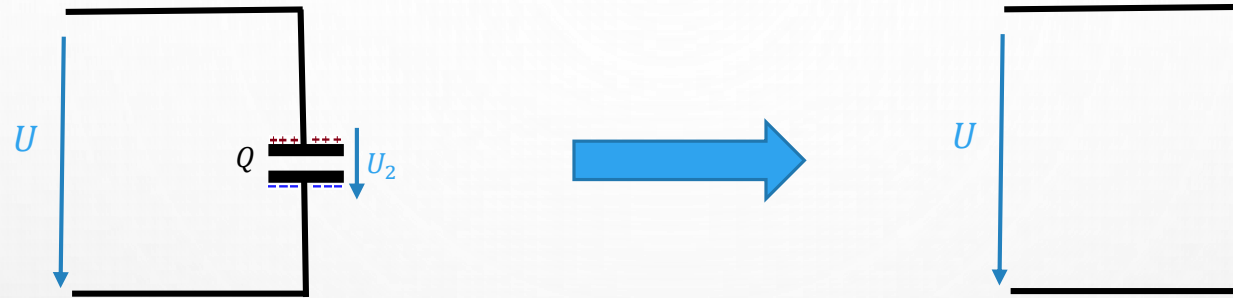
$$C_{tot} = C_1 + C_2$$

Gleiche Spannung
über allen Platten!!

BEISPIEL

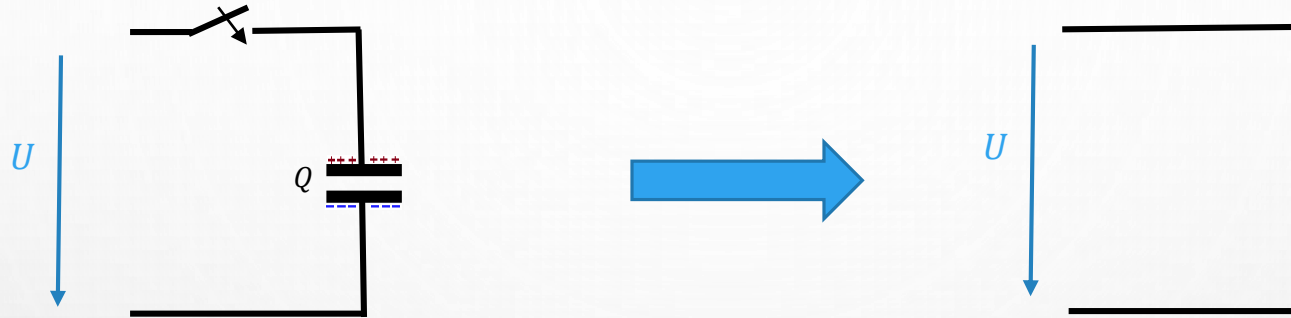


KONDENSATOR IM GLEICHSTROM

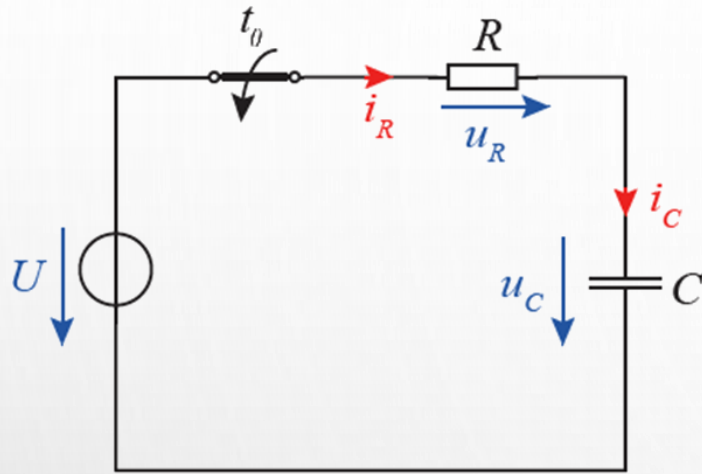


$$C \cdot \frac{\partial}{\partial t} U = 0 = I(t)$$

KONDENSATOR BEI EINSCHALTVORGÄNGEN



$$C \cdot \frac{\partial}{\partial t} U = \infty = I(t)$$



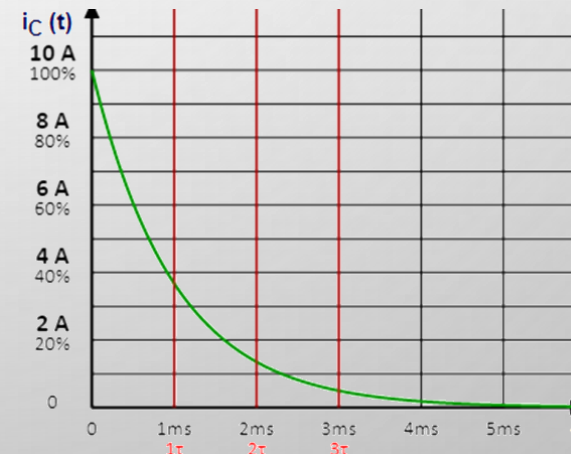
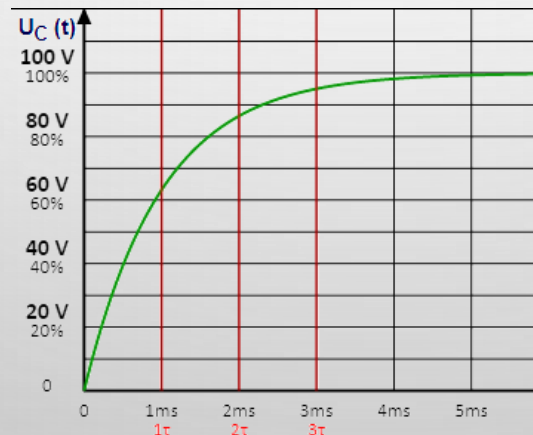
TRANSIENTE

Vor Schaltvorgang

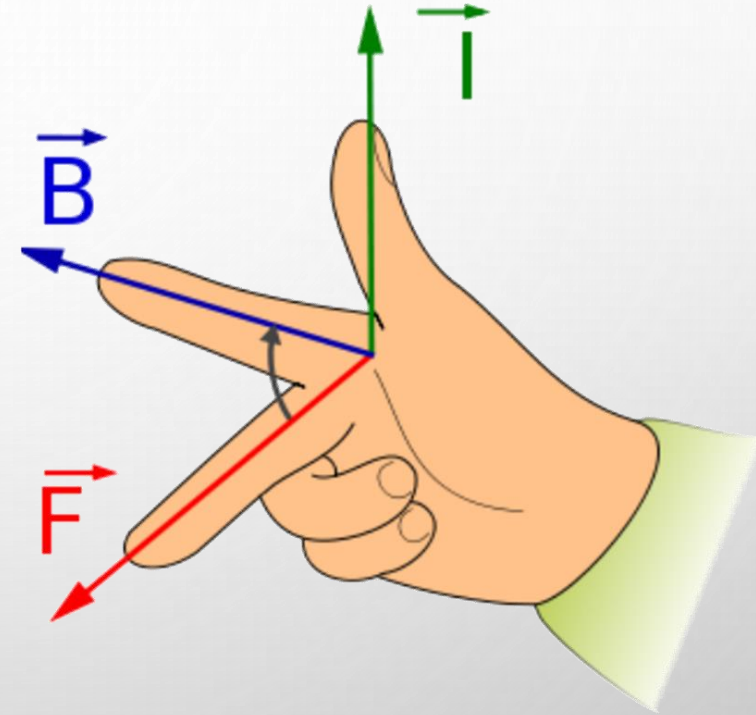
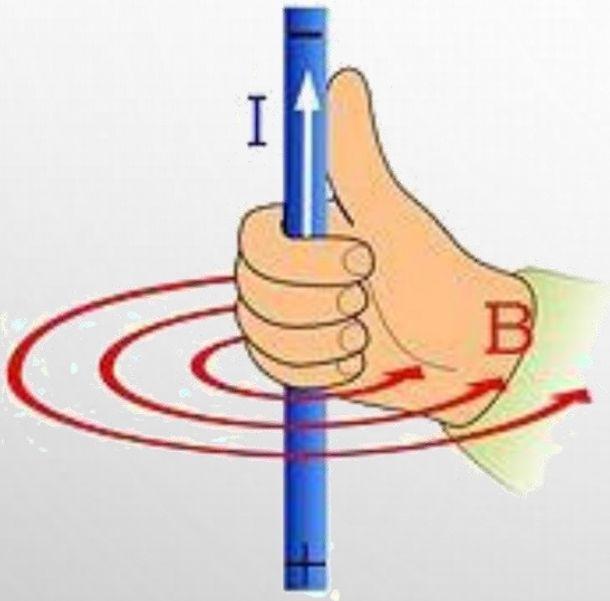
Nach Schaltvorgang

$$u_C(t) = u_C(t \rightarrow \infty) - [u_C(t \rightarrow \infty) - u_C(t = t_0)] \cdot \exp\left(-\frac{t - t_0}{RC}\right)$$

$$i_C(t) = \frac{1}{R} [u_C(t \rightarrow \infty) - u_C(t = t_0)] \cdot \exp\left(-\frac{t - t_0}{RC}\right)$$



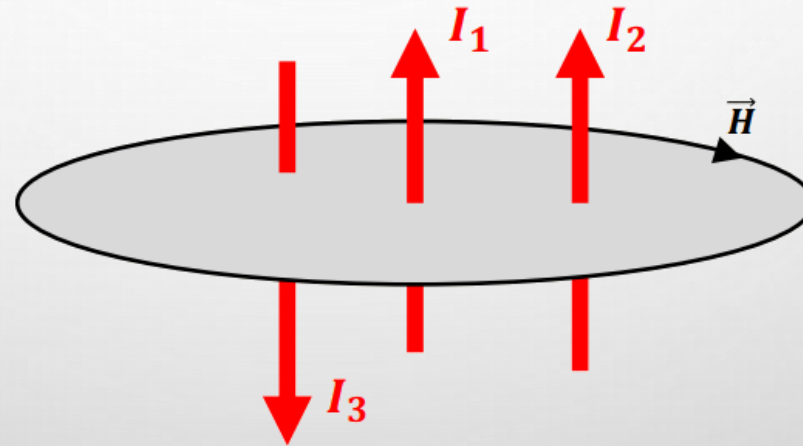
MAGNETFELD



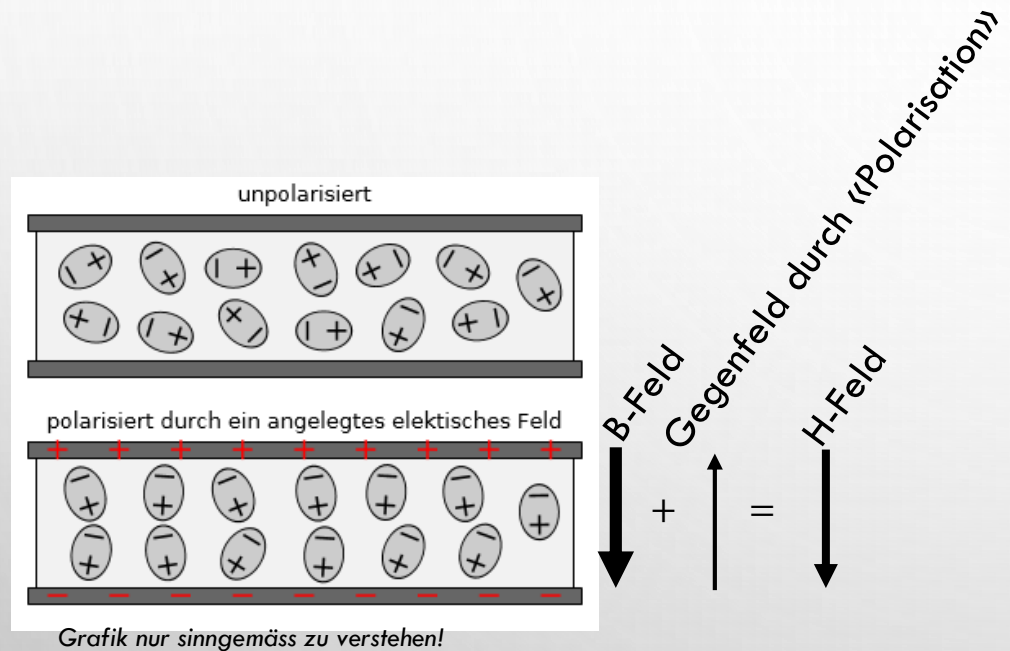
DURCHFLUTUNGSSATZ

$$\oiint_{\partial A} \mathbf{H} \cdot d\mathbf{s} = \oiint_{\partial A} \frac{B}{\mu} \cdot d\mathbf{s} = \iint_A \mathbf{j} \cdot d\mathbf{A} = \Theta y$$

«Fliesst Strom durch eine Fläche, so entsteht ein Magnetfeld $\mathbf{H}$ dessen Wert ähnlich zur Fläche und Stromstärke ist»



FLUSSDICHTE / FELDSTÄRKE

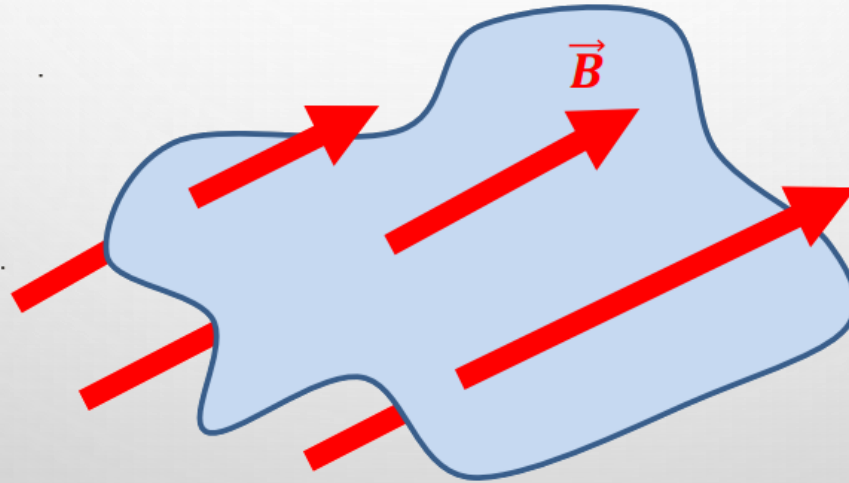


B-Feld: Konstante Grösse

H-Feld: Hängt vom Material ab.
In perfekten Magneten $H \rightarrow 0$

MAGNETISCHER FLUSS

$$\Phi = \iint_A \mathbf{B} \cdot d\mathbf{A} = \iint_A \frac{\mathbf{B}}{\mu} \cdot d\mathbf{A}$$



RELUKTANZMODEL

Spannung

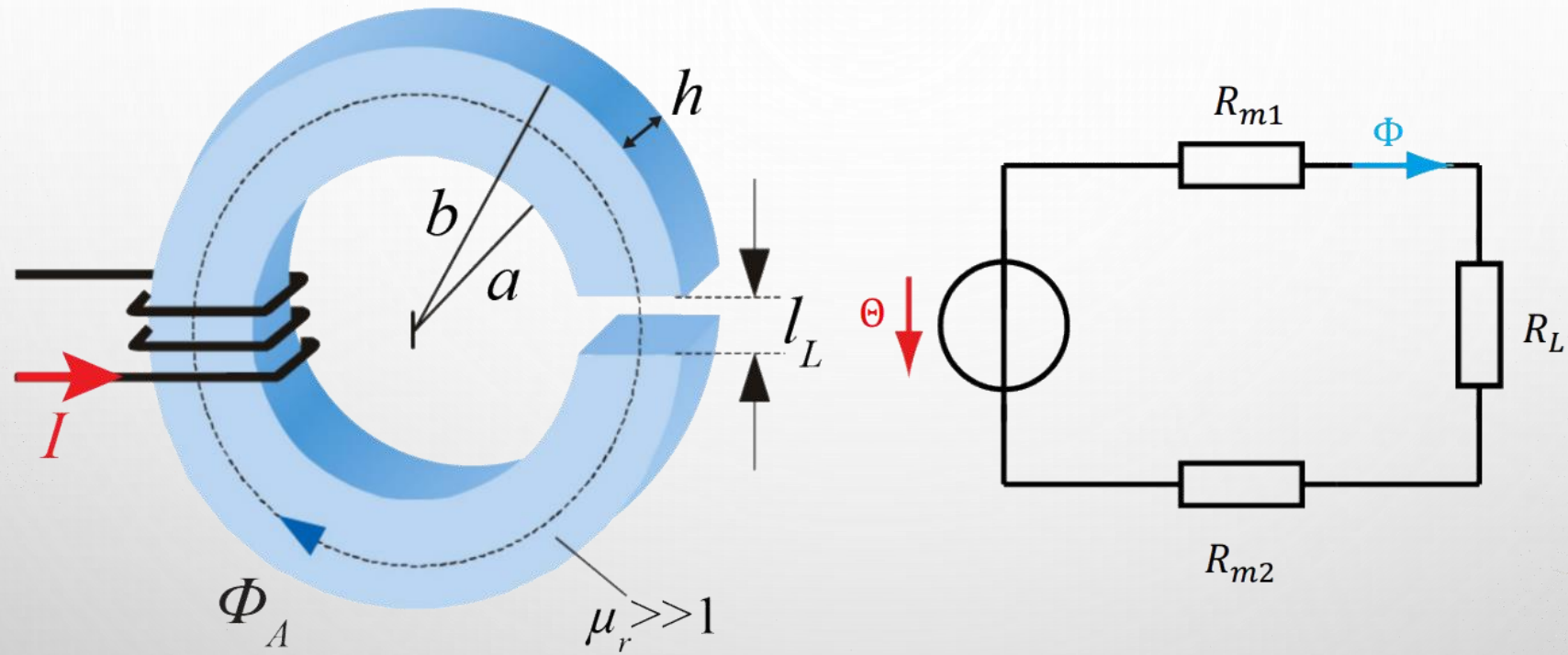
$$V_M = \theta = N \cdot I = \int \mathbf{H} \cdot d\mathbf{s} \qquad U = \int \mathbf{E} \cdot d\mathbf{s}$$

Strom

$$\Phi = \iint_A \mathbf{B} \cdot d\mathbf{A} \qquad I = \iint_A \kappa \mathbf{E} \cdot d\mathbf{A}$$

Widerstand

$$R_m = \frac{\theta}{\Phi} = \frac{l}{\mu A} \qquad R = \frac{U}{I}$$



INDUKTIVITÄT

Wie viel Magnetischer Fluss Φ baut sich bei einem Spulenstrom von I im Kernmaterial auf?

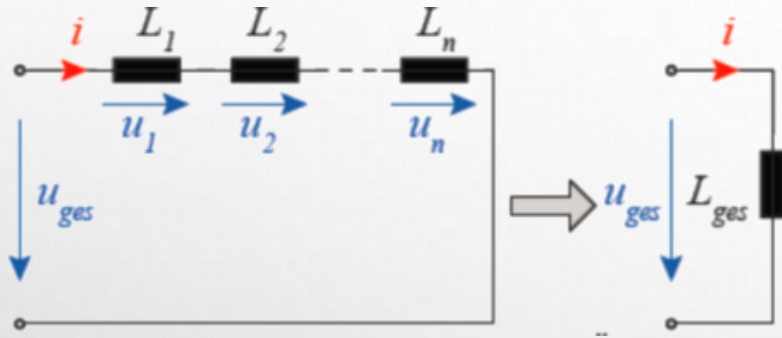
$$\text{Induktivität: } L = N \cdot \frac{\Phi}{I} = \frac{N \cdot \theta}{R_M \cdot I} = \frac{N^2}{R_M}$$

$$\text{Energie: } \frac{1}{2} L I^2$$

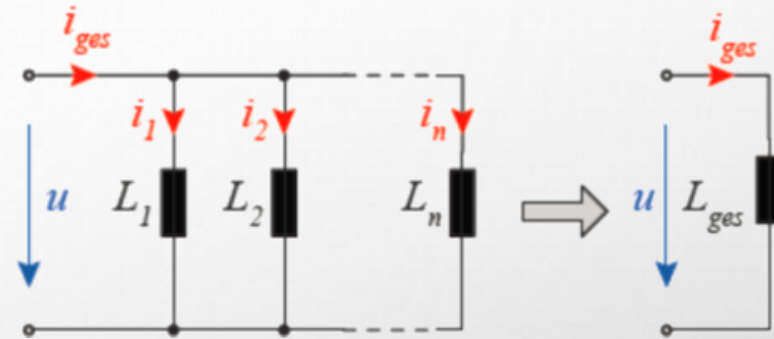


Serienschaltung

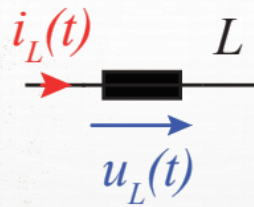
$$L_{ges} = \sum_i L_i$$

**Parallelschaltung**

$$L_{ges} = (L_1 || \dots || L_n) = \left[\sum_i \frac{1}{L_i} \right]^{-1}$$



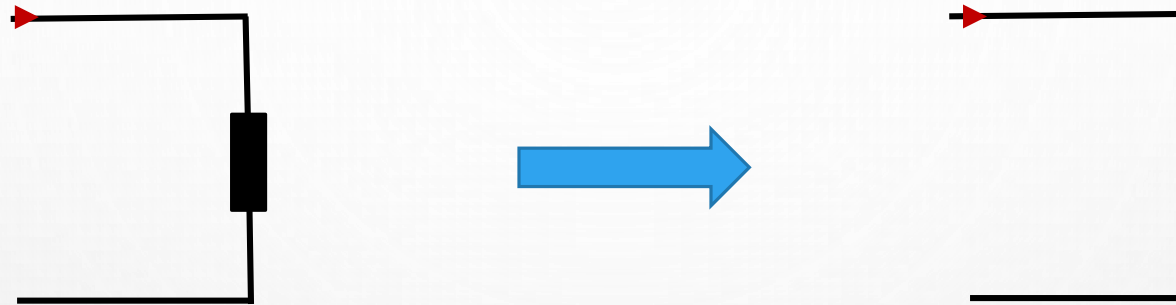
CHARAKTERISTISCHE GLEICHUNGEN



$$u(t) = L \frac{\partial}{\partial t} i(t)$$

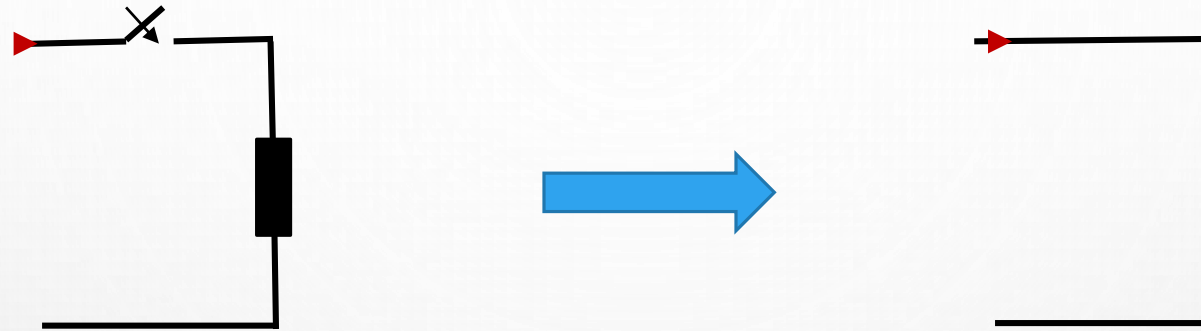
$$i(t) = \frac{1}{L} \int u(t) dt$$

INDUKTIVITÄT IM GLEICHSTROM

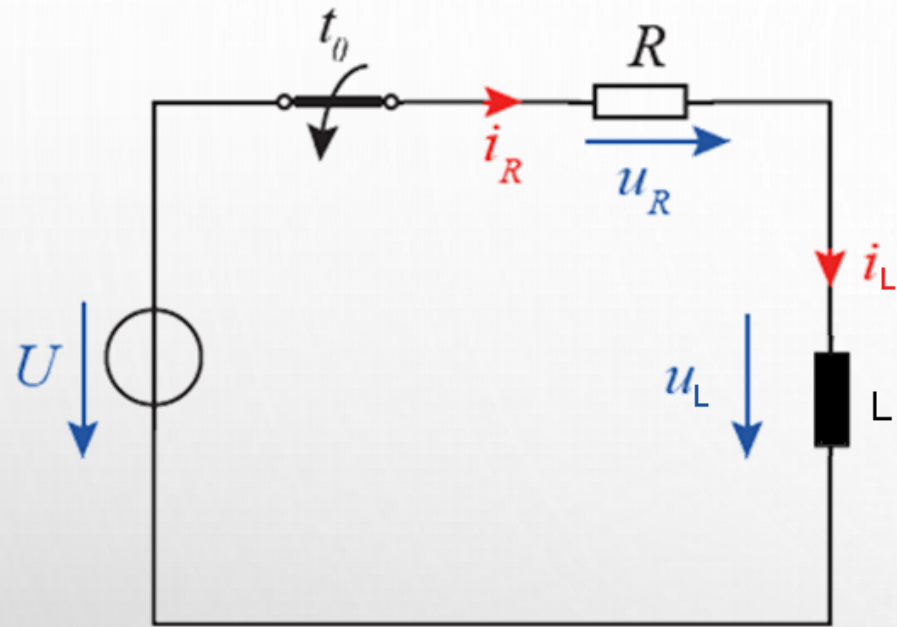


$$L \cdot \frac{\partial}{\partial t} i(t) = 0 = U(t)$$

INDUKTIVITÄT BEI EINSCHALTVORGÄNGEN



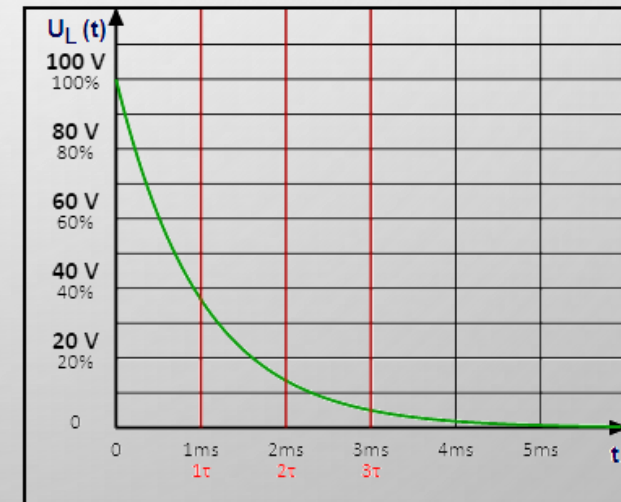
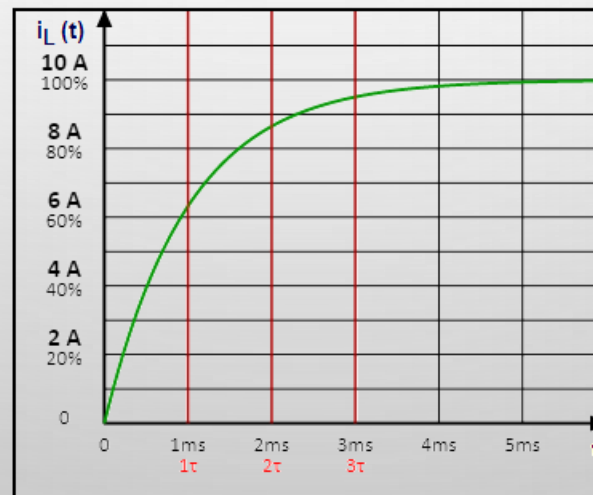
$$L \cdot \frac{\partial}{\partial t} i(t) = \infty = U(t)$$



TRANSIENTE

$$U_L(t) = R[I_L(t \rightarrow \infty) - I_L(t = t_0)] \cdot \exp\left(-R \frac{(t-t_0)}{L}\right)$$

$$I_L(t) = I_L(t \rightarrow \infty) - [I_L(t \rightarrow \infty) - I_L(t = t_0)] \cdot \exp\left(-R \frac{(t-t_0)}{L}\right)$$



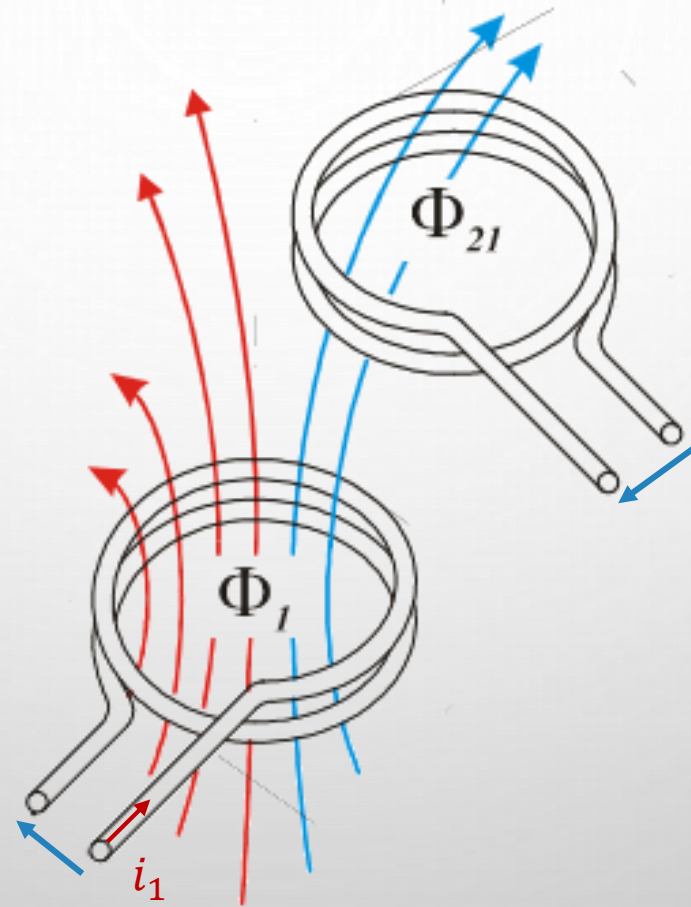
MAGNETISCHE KOPPELUNG

$$U_2 = N_2 \cdot \frac{d\Phi_{21}}{dt}$$

$$U_2 = L_{21} \cdot \frac{di_1}{dt}$$

$$U_1 = L_{12} \cdot \frac{di_2}{dt}$$

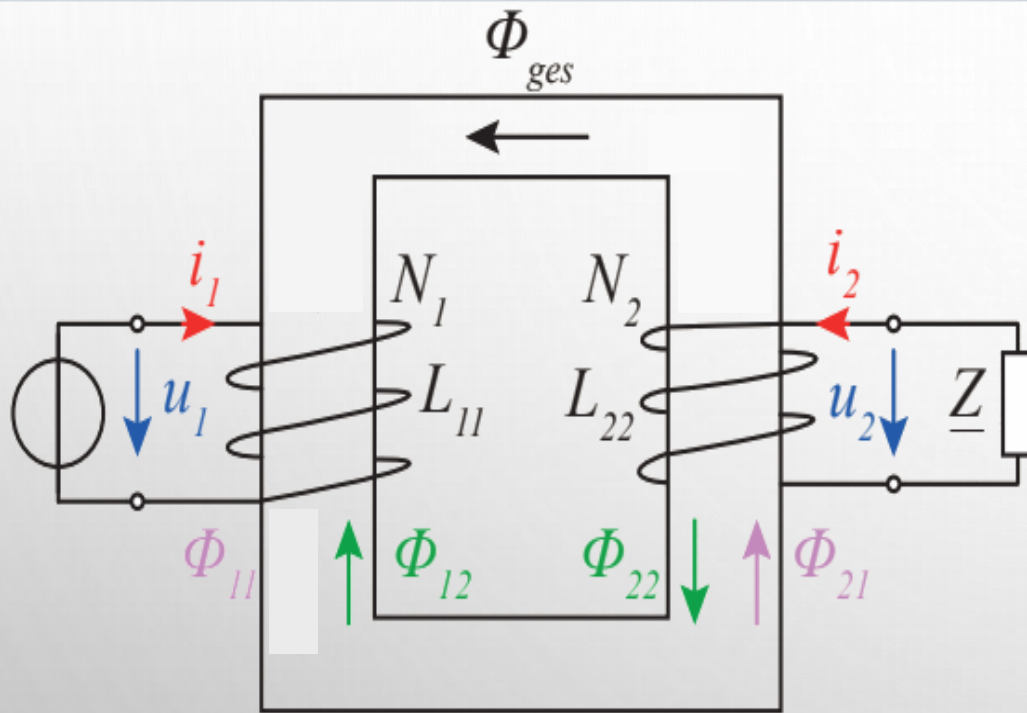
$$L_{12} = L_{21} = M$$



Magnetische Kopplung M :

Wieviel Magnetfeld baut sich in Spule **2** auf, wenn ich einen gewissen Strom durch Spule **1** fließen lasse

ÜBERTRAGER



$$u_1 = N_1 \frac{d}{dt} (\Phi_{11} - \Phi_{12}) = L_{11} \frac{di_1}{dt} - L_{12} \frac{di_2}{dt} = L_{11} \frac{di_1}{dt} - M \frac{di_2}{dt}$$

$$u_2 = N_2 \frac{d}{dt} (-\Phi_{21} - \Phi_{22}) = -L_{21} \frac{di_1}{dt} - L_{22} \frac{di_2}{dt} = -M \frac{di_1}{dt} + L_{22} \frac{di_2}{dt}$$

Falls keine Verluste:

$$\Phi_{ges} = \Phi_{11} - \Phi_{12} = \Phi_{21} - \Phi_{22}$$

$$\Phi_{11} = \Phi_{21}, \Phi_{22} = \Phi_{12}$$

$$u_1 = N_1 \frac{d\Phi_{ges}}{dt}$$

$$u_2 = -N_2 \frac{d\Phi_{ges}}{dt}$$

$$\frac{u_1}{u_2} = \frac{N_1}{N_2}$$

IDEALER ÜBERTRAGER

Ideal $\rightarrow$ Keine Verluste

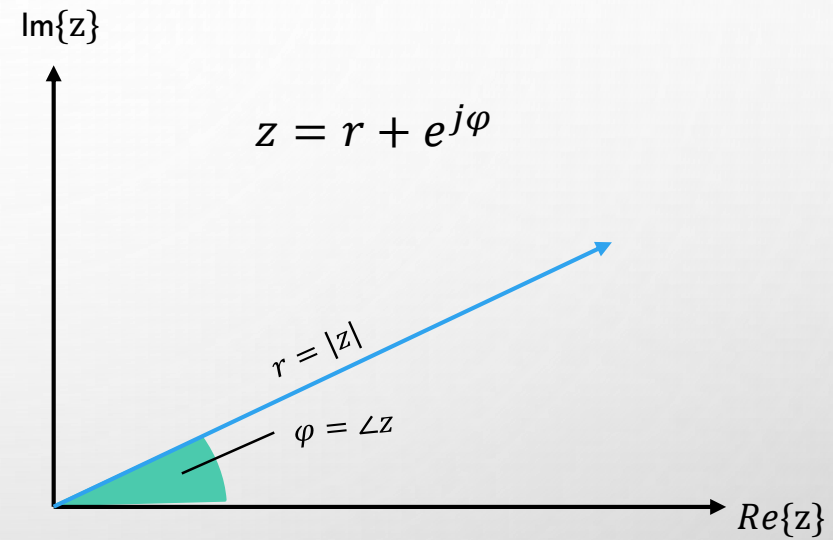
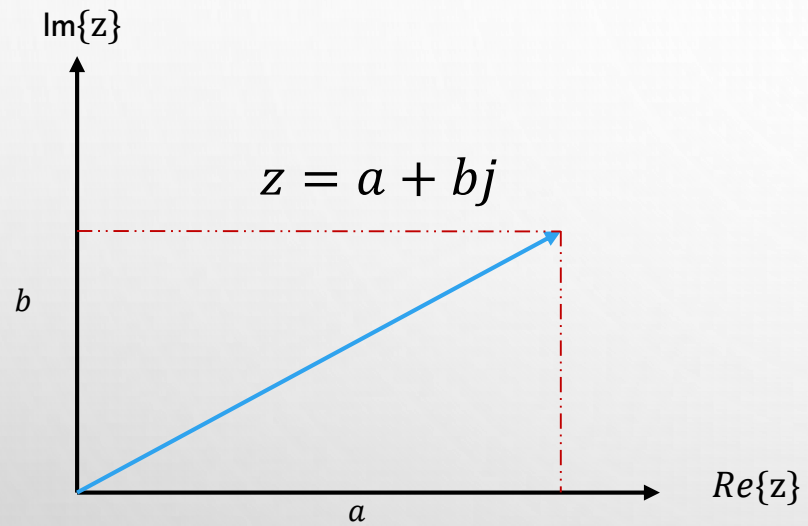
$$\mu_r \rightarrow \infty$$

$$R_m \rightarrow 0$$

$$P_{in} = P_{out}$$

$$\frac{i_1}{i_2} = \frac{N_2}{N_1}$$

KOMPLEXE ZAHLEN



RECHNEN MIT KOMPLEXEN ZAHLEN

$$\operatorname{Im}\{Z_1\} = \frac{1}{2}(Z_1 - Z_1^*)$$

$$\operatorname{Re}\{Z_1\} = \frac{1}{2}(Z_1 + Z_1^*)$$

$$Z_1 = a + bj \rightarrow Z_1^* = a - bj$$

$$|Z_1| = \sqrt{a^2 + b^2} = r$$

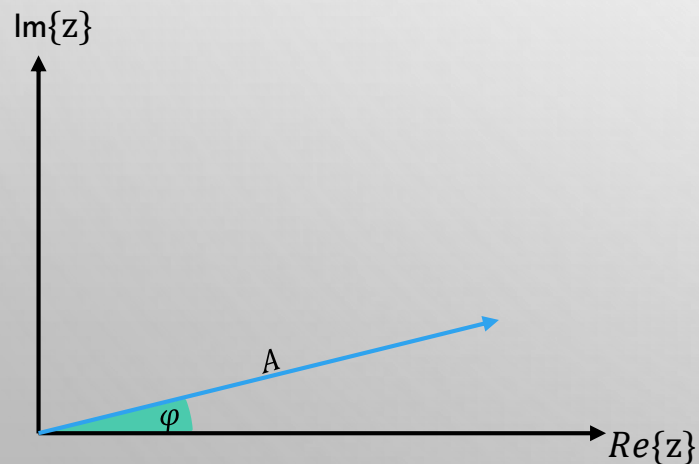
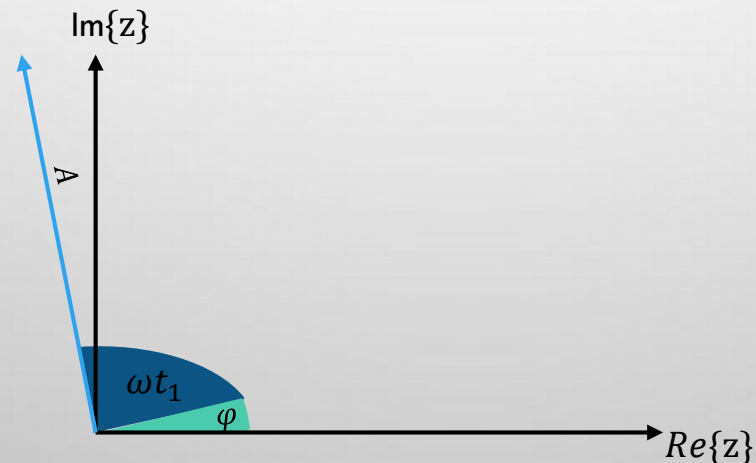
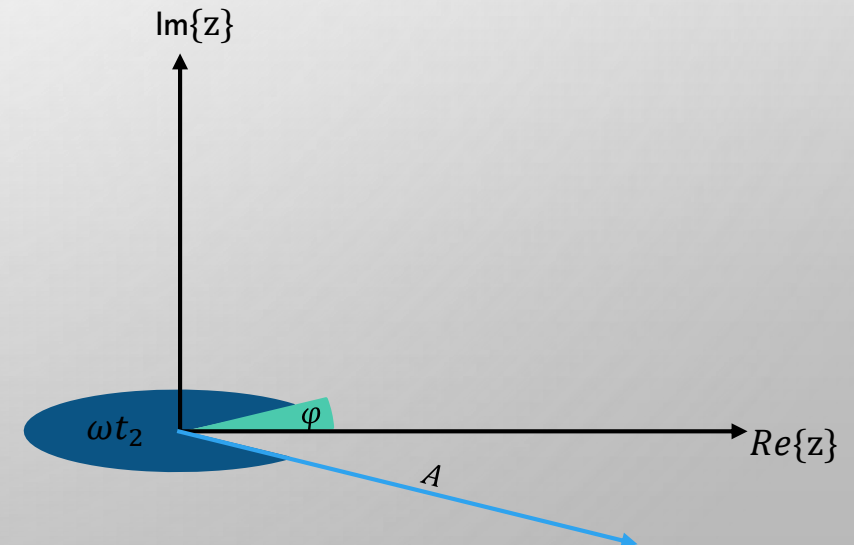
$$\frac{Z_1}{Z_2} = \frac{Z_1 \cdot Z_2^*}{Z_2 \cdot Z_2^*} = \frac{Z_1 \cdot Z_2^*}{\operatorname{Re}\{Z_2\}^2 + \operatorname{Im}\{Z_2\}^2}$$

$$r \cdot e^{j\varphi} = r[\cos(\varphi) + j \cdot \sin(\varphi)]$$

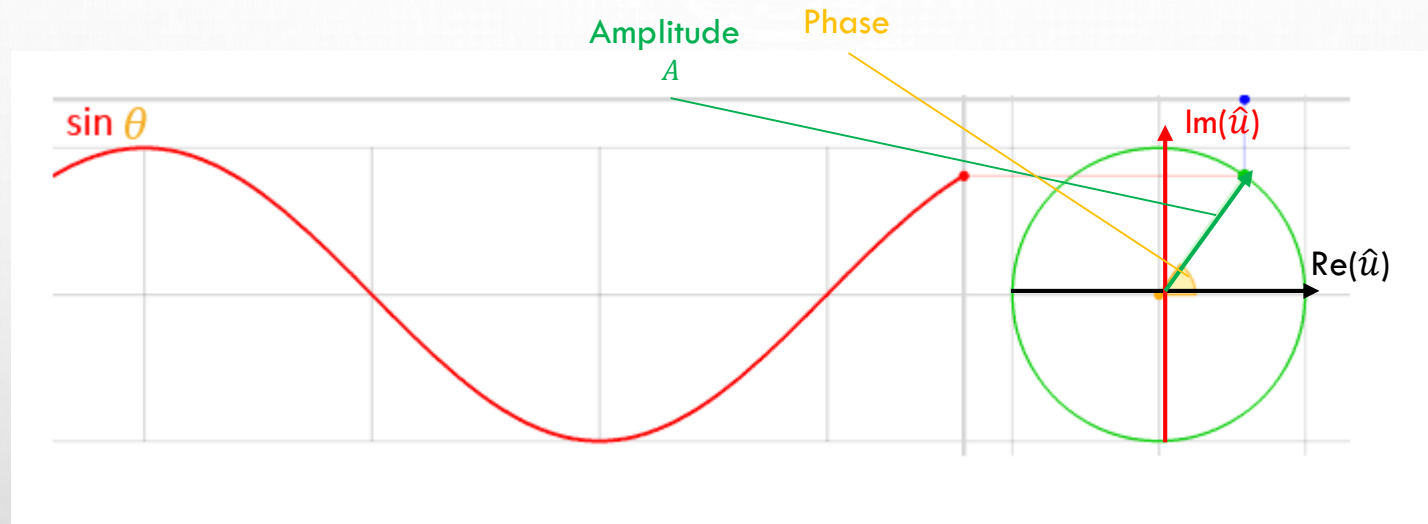
ROTIERENDE ZEIGER

$$Z(t) = A_0 \cdot e^{j\omega t}$$

$$A_0 = A \cdot e^{j\varphi}$$

 $Z(t = 0)$  $Z(t = t_1 \approx \frac{\pi}{2} \cdot \frac{1}{\omega})$  $Z(t = t_2)$ 

KOMPLEXE ZEIGER



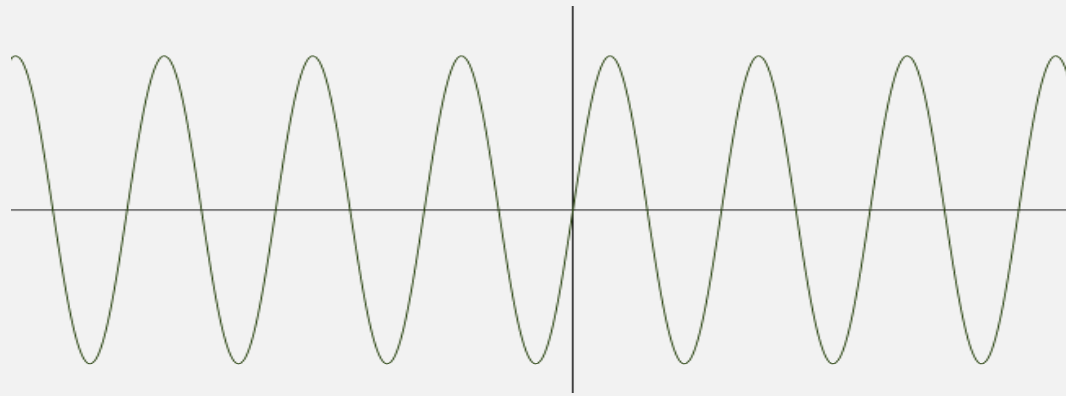
$$A \cdot \sin(\omega t) = \text{Im} \{ A \cdot e^{j\omega t} \}$$

$$A \cdot \sin(\omega t + \varphi) = \text{Im} \{ \underline{A} \cdot e^{j\omega t} \}$$

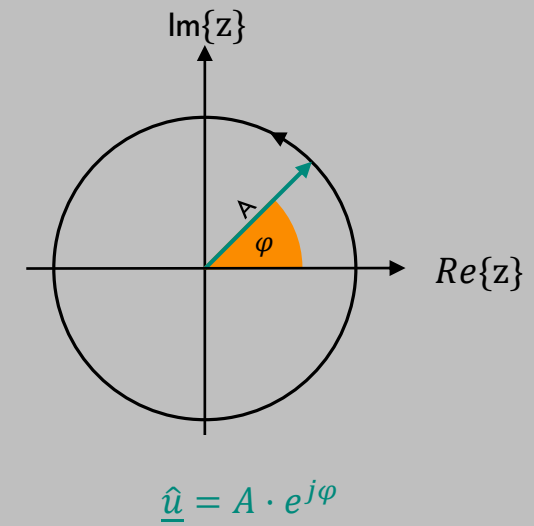
$$\underline{A} = A \cdot e^{j\varphi}$$

Realer Raum

$$u(t) = A \cdot \sin(\omega t + \varphi)$$

 $t = 0$
→

Komplexer Raum (Zeitunabhängig)

 $\leftarrow \text{Im}\{\underline{\hat{u}} \cdot e^{j\omega t}\}$

VERSCHIEDENE ZEIGER

Signal: $u(t) = A \cdot \sin(\omega t + \varphi)$

Effektivwert: $U = \sqrt{\frac{1}{T} \int_0^T u(t)^2 dt}$

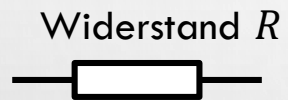
Symbol	Bedeutung
$\hat{u}$	Spitzen/Amplitudenwert (=A)
U	Effektivwert ($\frac{1}{\sqrt{2}} \cdot \hat{u}$)
$\underline{U}$	Komplexer Zeiger (Effektivwert)
$\underline{\hat{u}}$	Komplexer Zeiger (Spitzenwert)

IMPEDANZ

Transformiere $u(t) = L_o(i(t))$ in den komplexen Raum

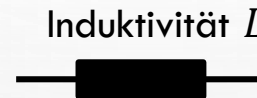
$$\frac{\partial}{\partial t} e^{j\omega t} = j\omega$$

$$\int e^{j\omega t} dt = \frac{1}{j\omega}$$



$$u(t) = R \cdot i(t)$$

$$\underline{U} = \boxed{R} \cdot \underline{I}$$



$$u_L(t) = L \cdot \frac{\partial}{\partial t} i_L(t)$$

$$\underline{U} = \boxed{j\omega L} \cdot \underline{I}$$



$$u_L(t) = \frac{1}{C} \cdot \int i_L(t) dt$$

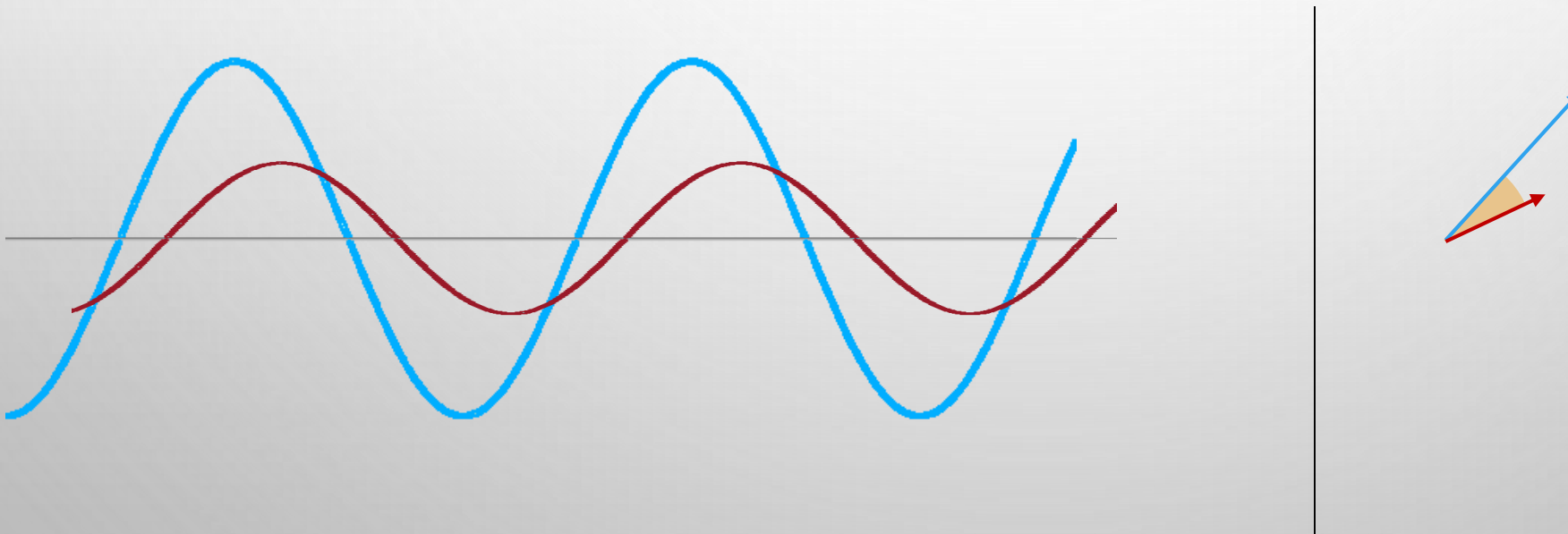
$$\underline{U} = \boxed{\frac{1}{j\omega C}} \cdot \underline{I}$$

LINEARE NETZWERKE

Lineare Netzwerke verändern die Frequenz des Sinus nicht

Es ändert sich nur

- Phase φ
- Amplitude



IMPEDANZ

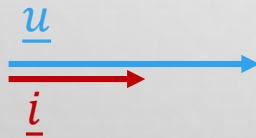
Widerstand R



$$\underline{Z} = R$$

Strom und Spannung
in Phase

$$\Delta\varphi = 0$$



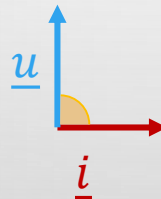
Induktivität L



$$\underline{Z} = j\omega L$$

In Induktivitäten die
Ströme sich verspäten

$$\Delta\varphi = -\frac{\pi}{2}$$



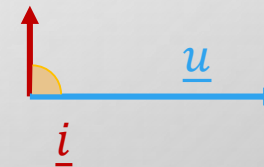
Kapazität C



$$\underline{Z} = 1/j\omega C$$

Der Strom eilt **vor**
im Kondensator

$$\Delta\varphi = \frac{\pi}{2}$$

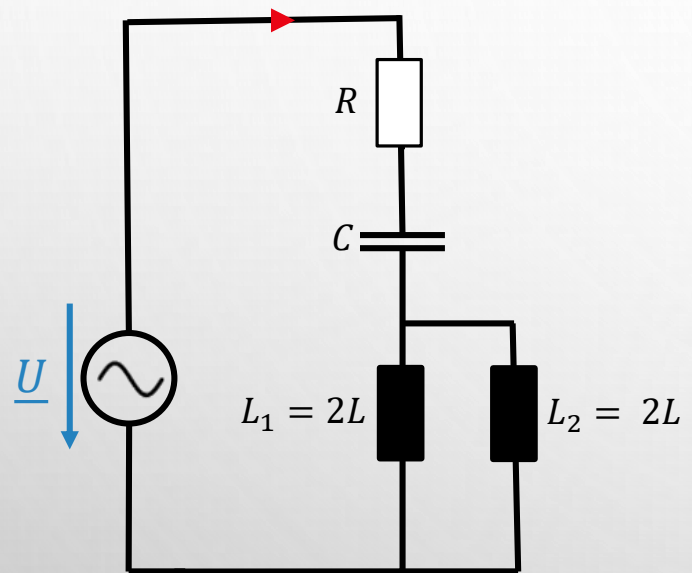


VORGEHEN

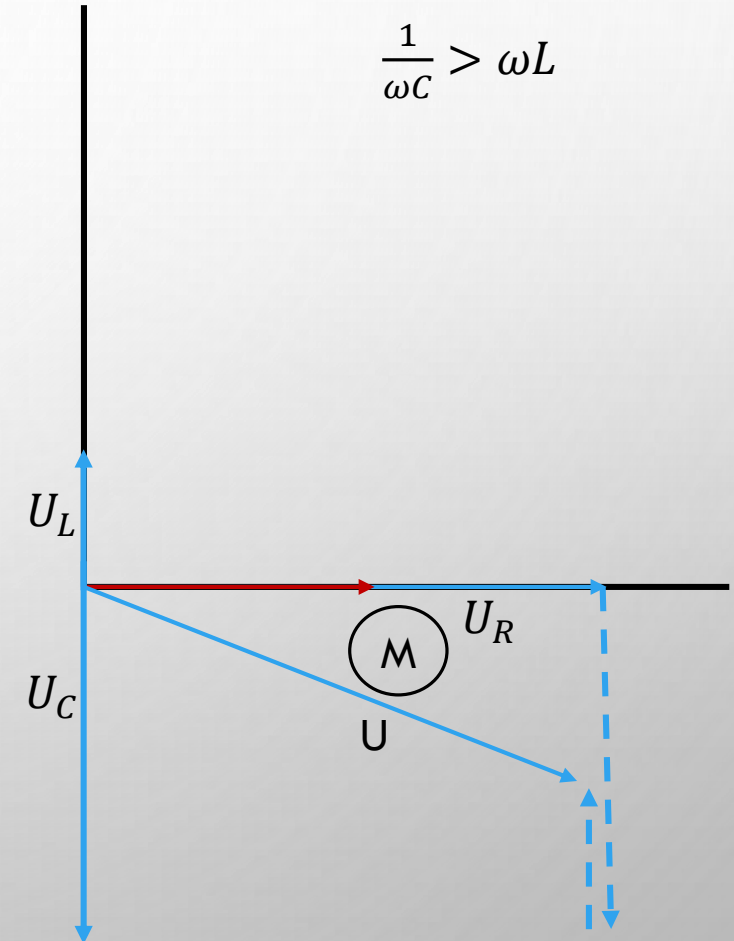
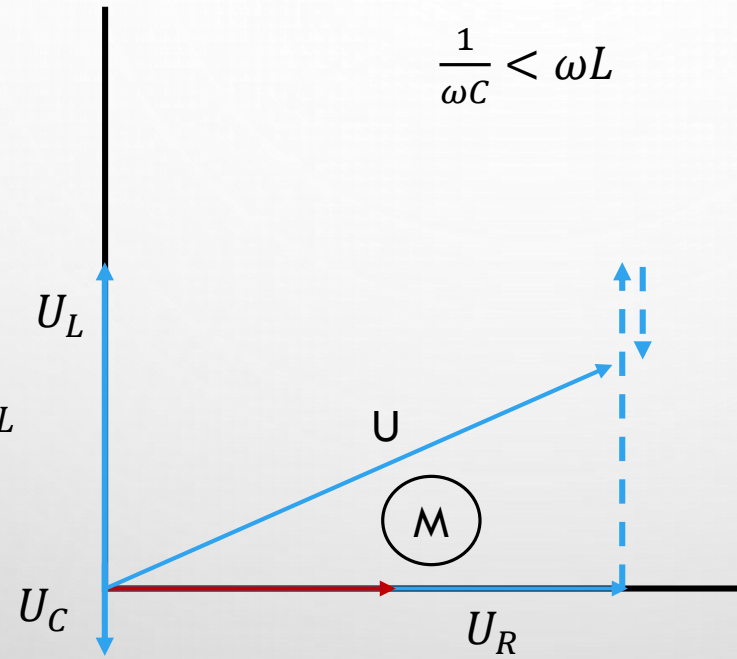
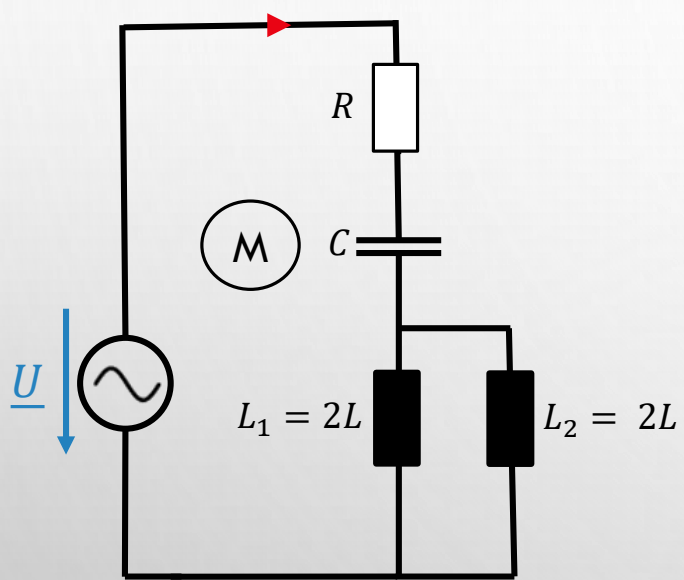
- Transformiere Schaltung in Komplexen Raum
 - Spannungen und Ströme werden zu Zeiger
 - Widerstände, Spulen und Kondensatoren zu Impedanzen
- Berechne die benötigten zeiger mittels spannungsteiler etc.
(Gleiche regeln für Impedanzen wie widerstände)
- Transformiere zurück falls verlangt

BEISPIEL

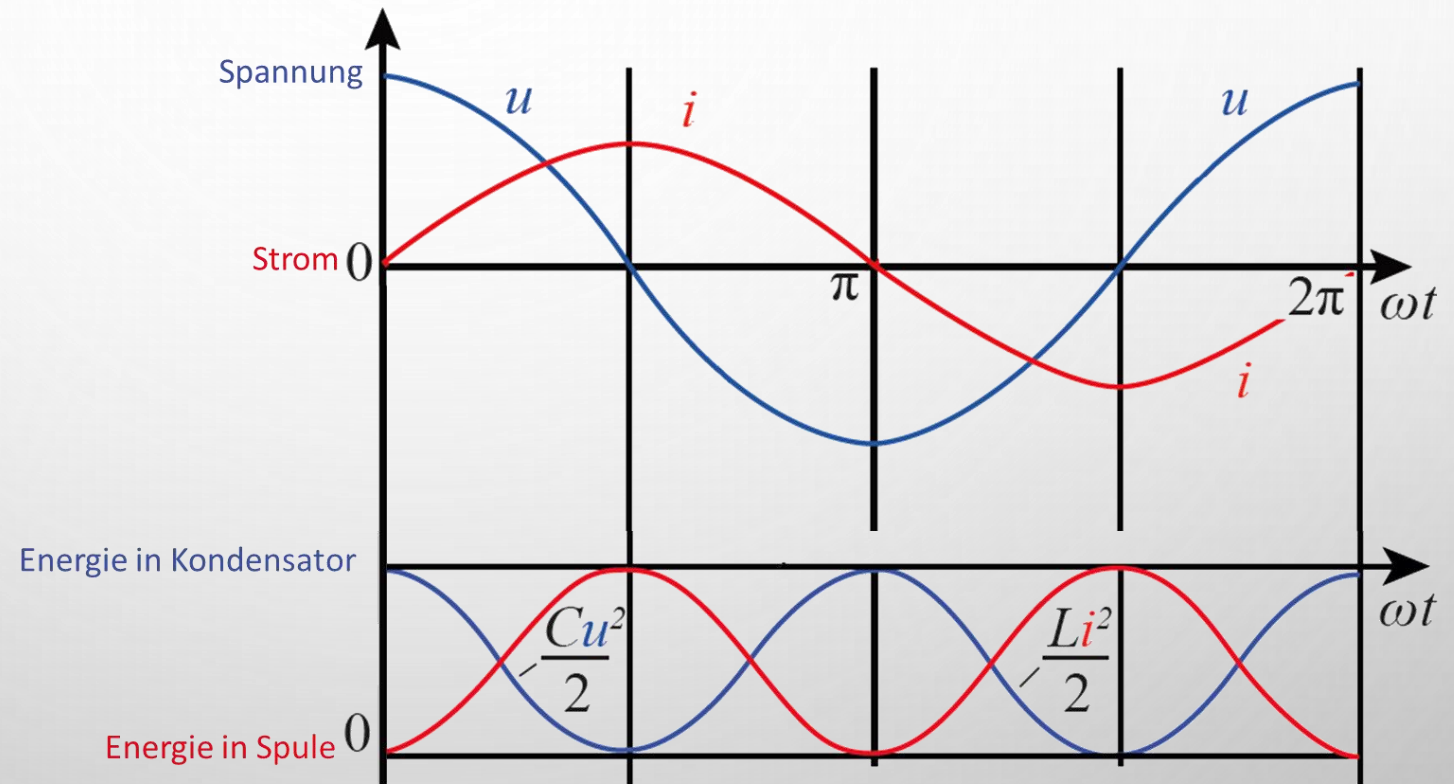
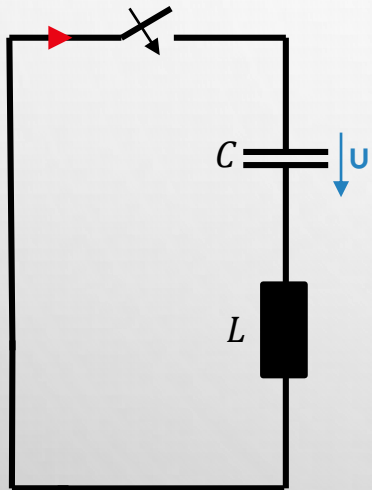
Berechne alle Spannungen in Abhängigkeit von U , R , L , C und ω



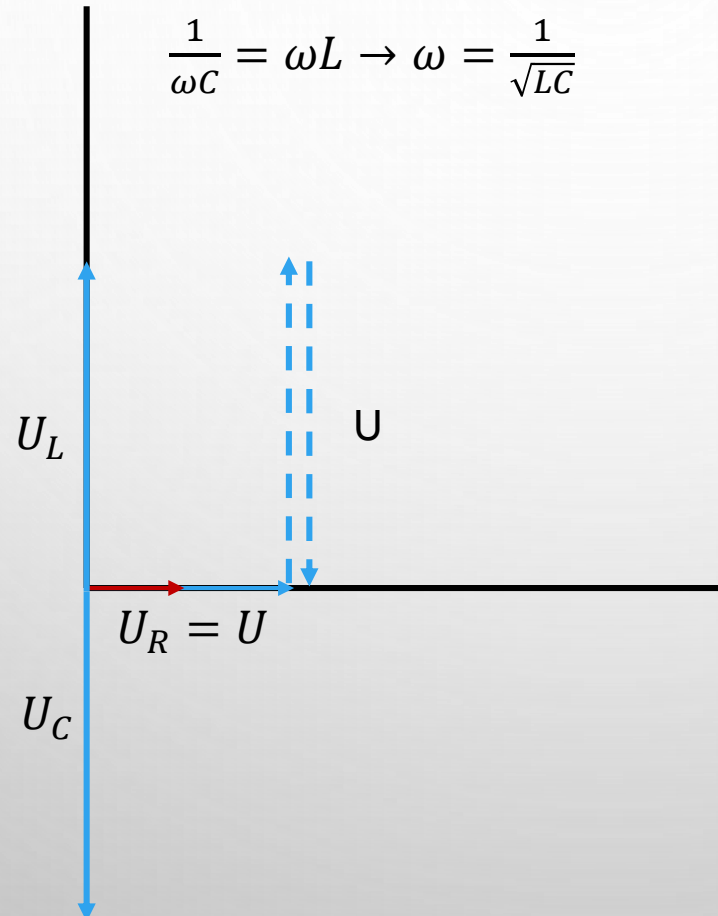
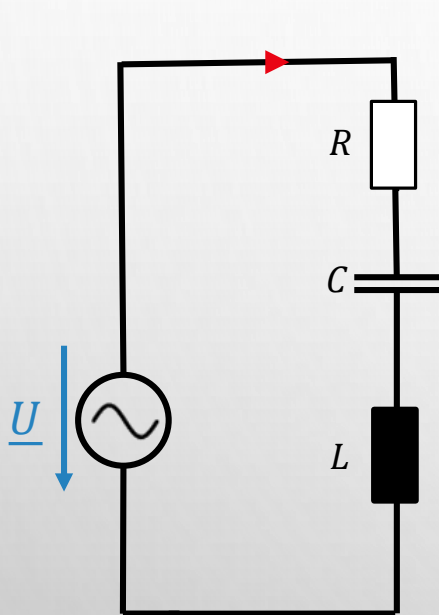
ZEIGERDIAGRAMM



SCHWINGKREISE



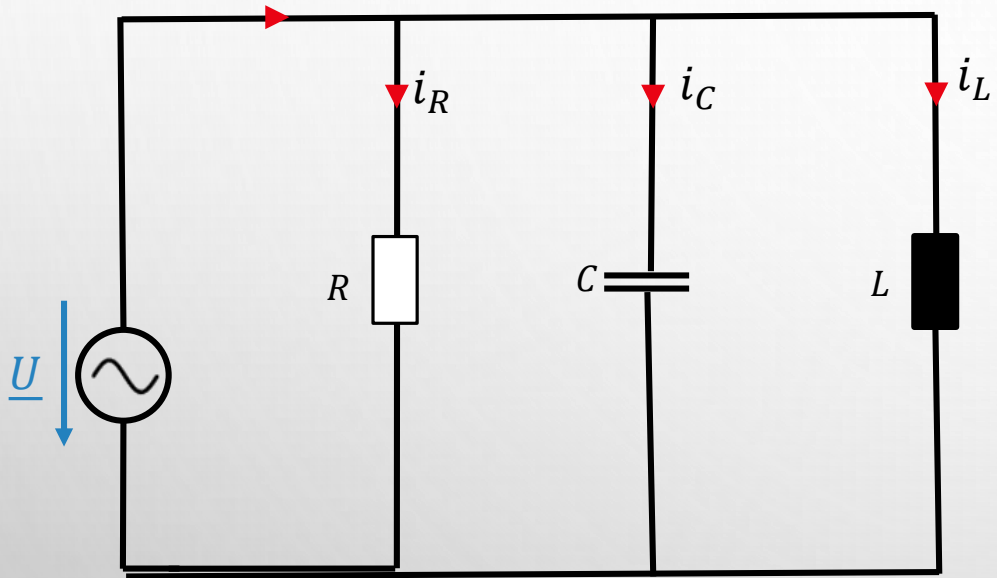
SCHWINGKREISE



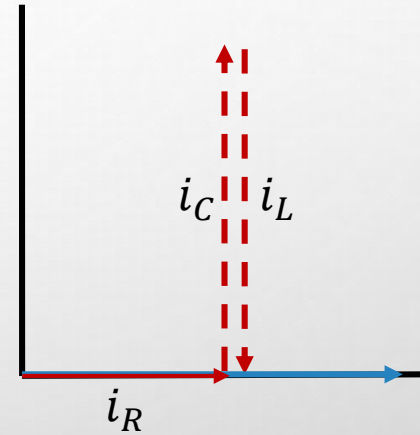
$$\underline{U_c} = \underline{U} \cdot \frac{1}{j\omega CR + 1 - \omega^2 CL} = \underline{U} \cdot \frac{1}{j\omega C \cdot R}$$

$$\rightarrow \angle(U_c - U) = 90^\circ$$

SCHWINGKREISE



$$\omega = \frac{1}{\sqrt{LC}}$$

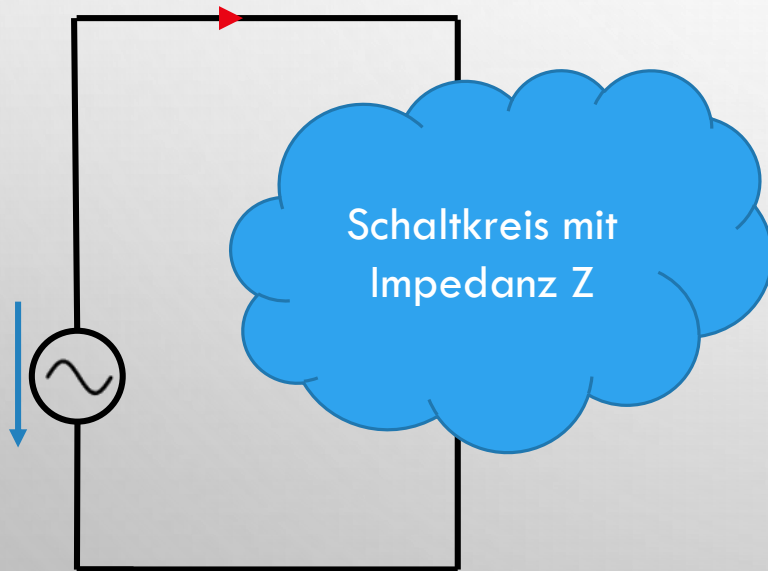


SCHWINGKREISE

Sobald ein Kondensator und eine Spule in einer Schaltung vorhanden sind, können Schwingungen auftreten

Bei Resonanzfrequenz können Spannungs/Stromüberhöhungen auftreten.

Strom und Spannung der Quelle sind dabei in Phase



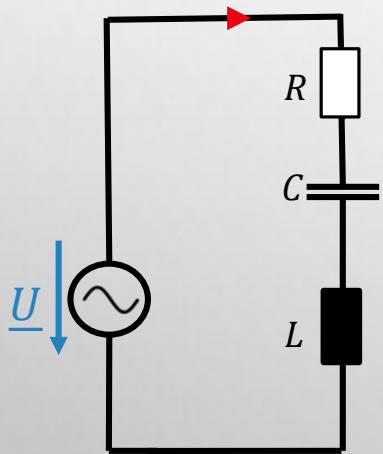
Resonanz:

U und I in Phase $\rightarrow U = Z \cdot I = \operatorname{Re}\{Z\} \cdot I$

Z ist Reell $\leftrightarrow Y = \frac{1}{Z}$ ist Reell

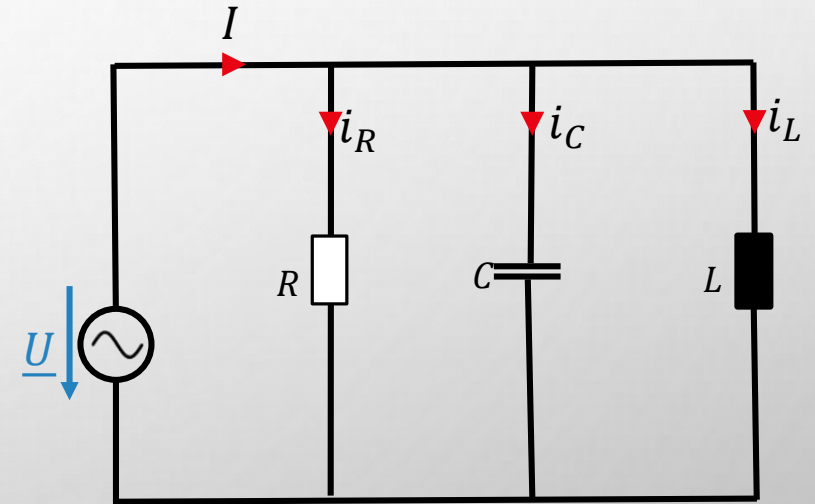
GÜTE

Leistung in Schwingkreis
Leistungsverlust pro Periode

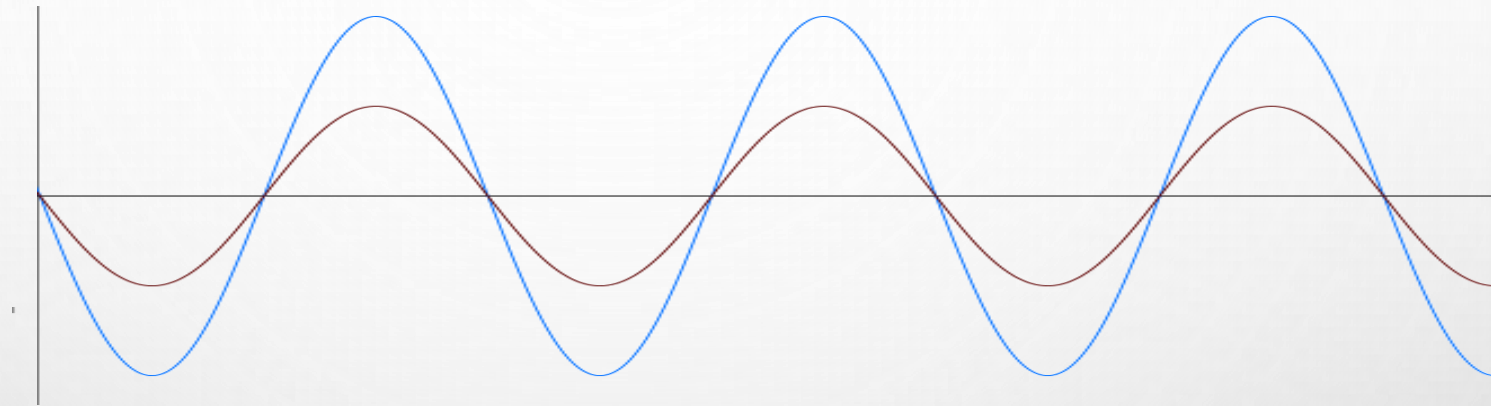
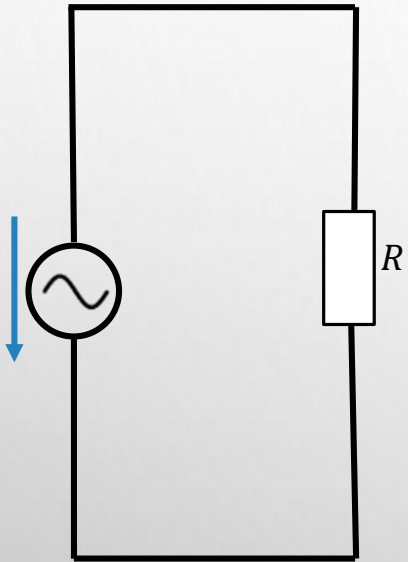


$$Q_S \approx \frac{U_L}{U} = \frac{U_C}{U}$$

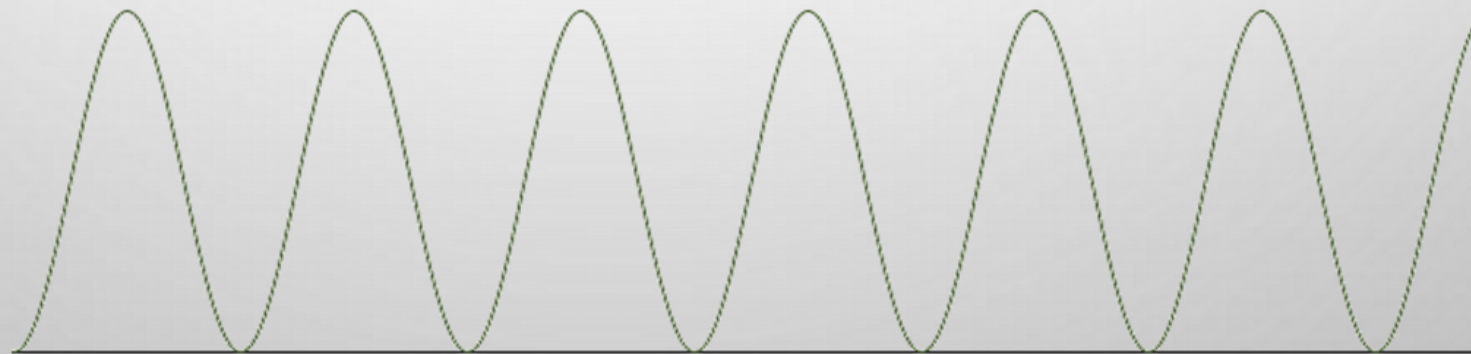
$$Q_P \approx \frac{i_C}{I} = \frac{i_L}{I}$$



WIRKLEISTUNG = P

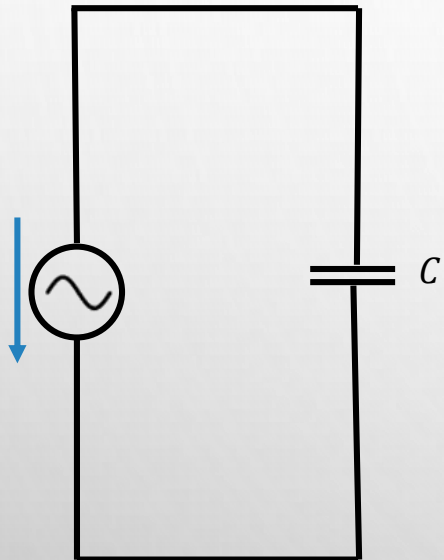


$$p(t) = u(t) \cdot i(t)$$

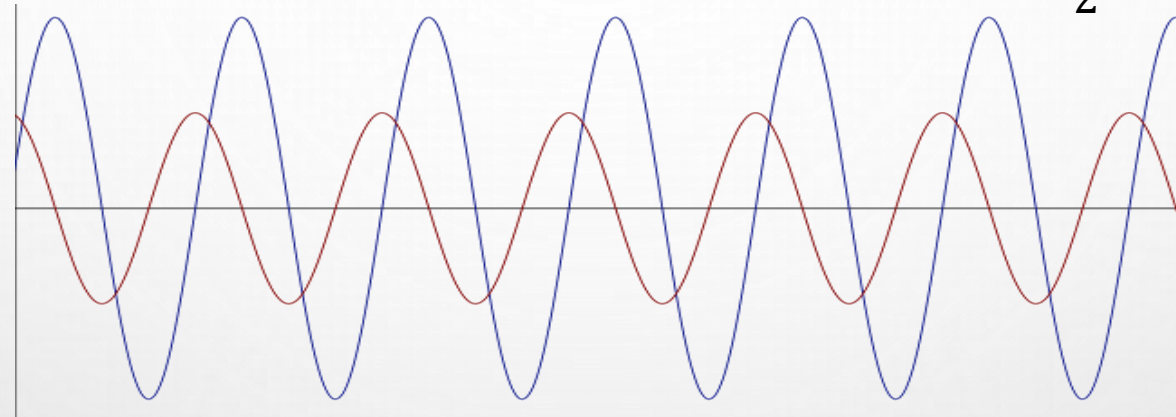


$$\langle p(t) \rangle = U \cdot I$$

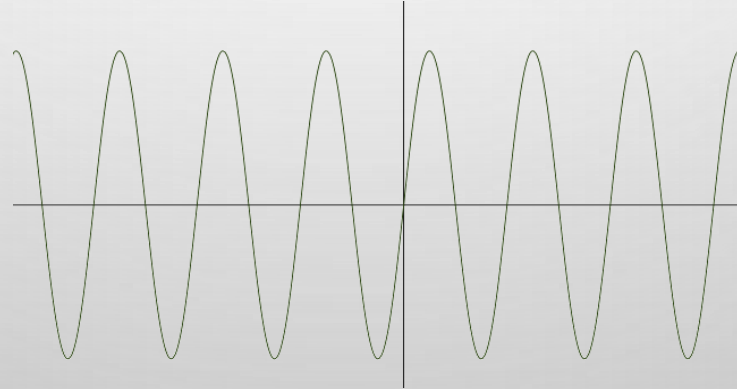
BLINDLEISTUNG = Q



$$u(t) = A \cdot \sin(\omega t), \quad i(t) = B \cdot \cos\left(\omega t + \frac{\pi}{2}\right)$$

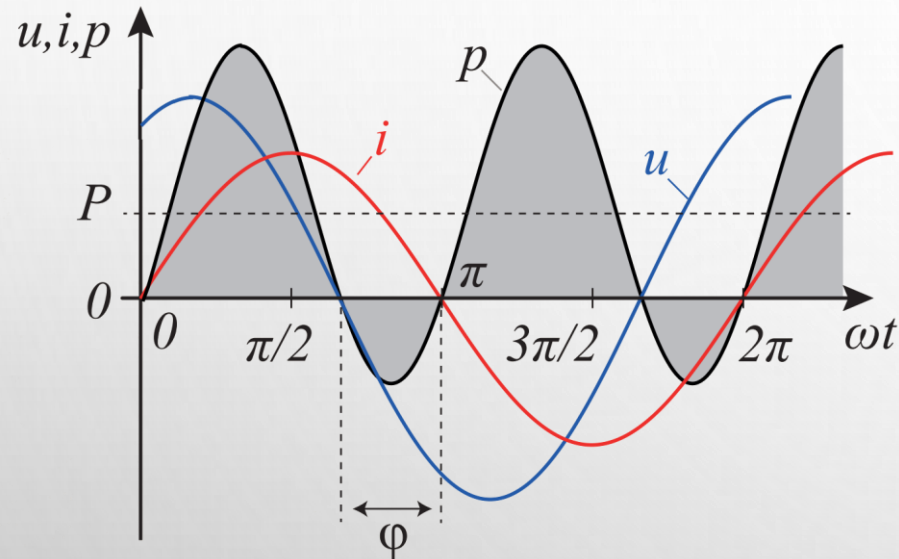


$$p(t) = u(t) \cdot i(t)$$



$$\langle p(t) \rangle = 0$$

KOMPLEXE LEISTUNG



$$\underline{S} = P + jQ = \underline{U} \cdot \underline{I}^*$$

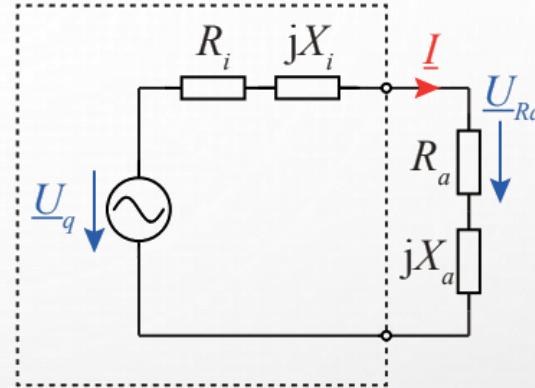
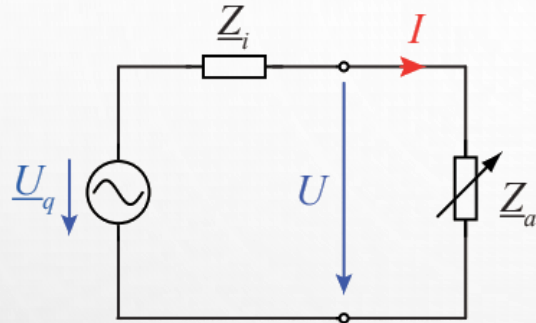
$$P = \operatorname{Re}\{\underline{S}\} = UI \cdot \cos(\varphi)$$

$$Q = \operatorname{Im}\{\underline{S}\} = UI \cdot \sin(\varphi)$$

Mit $\varphi = |\angle(\underline{U} - \underline{I})|$

$$\lambda := \frac{P}{|\underline{S}|} = \cos(\varphi)$$

LEISTUNGSANPASSUNG

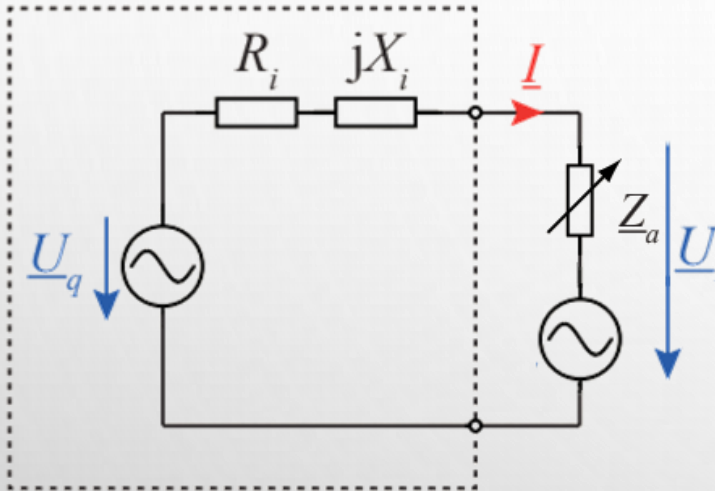


$$P = I^2 R_a = \frac{U_q^2 R_a}{(R_i + R_a)^2 + (X_i + X_a)^2}$$

$$X_a = -X_i$$

$$\underline{Z}_a = \underline{Z}_i^*$$

LEISTUNGSANPASSUNG



- Berechne $\underline{I}$ und $\underline{U}$ über der Last in Abhängigkeit von Z_a
- Maximale Wirkleistung:

$$\frac{\partial}{\partial(\operatorname{Re}\{Z_a\})} (\operatorname{Re}\{\underline{U} \cdot \underline{I}^*\}) = 0$$

- Minimale Blindleistung:

$$\frac{\partial}{\partial(\operatorname{Im}\{Z_a\})} (\operatorname{Im}\{\underline{U} \cdot \underline{I}^*\}) = 0$$

